# PHENOL removal in refinery wastewater using mixed oxides prepared by green synthesis

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#### ABSTRACT

Mixed solid oxides are known for their excellent catalytic property and applications in environmental remediation. This study presents a green-synthesis route for magnesium oxide–titanium oxide, a mixed oxide demonstrated to possess high performance of phenol removal from hydrocarbon refinery process wastewater. Mixed oxide (MgO-TiO2) was prepared by using the whole extract from leaves of Piliostigma Thonningii as a reducing agent. A structural attribute of the mixed oxide was investigated using X-ray Diffractometer, High-Resolution Scanning Electronic Microscopy and Energy Dispersive X-ray. Petroleum refinery raw wastewater having a phenol concentration of 19.961 mg/L was treated using green-synthesized mixed oxide. Adsorptive phenols removal up to 99.5% was achieved with a dosage of 0.04 g/100 mL at a temperature of 35 °C, and a contact time of 1.167 h. By this, the treated water meets the standard acceptable phenol concentration (0.1 mg/L) in wastewater of hydrocarbon refinery.

Keywords: Green synthesis; Magnesium oxide; Mixed oxide; Phenol; Process wastewater; Titanium oxide.

# **INTRODUCTION**

The environmental problem caused by organic pollutants, especially the phenolic compounds and their contributions to water pollution, have been widely reported in the literature (Vasudevan, 2014: Gupta & Balomajumder, 2015). It has been estimated that globally, over one billion people do not have access to safe drinking water. Meanwhile, pollutants due to industrialization have continually contaminated the available water sources by introducing substances (such as phenol) into the water bodies (Jinxia et al., 2019; Mais et al., 2019).

Phenolic compounds have generally been found to be one of the most dangerous organic pollutants in wastewater from the refinery. A very low amount of phenolic compounds in water still makes it highly toxic to human consumption (Mohamadi et al., 2015). In natural waters, phenol allows the formation of other toxic compounds through oxidation processes. In addition, the several methods used to remove phenols from wastewater have been observed to be confined because they often involve high capital and operational costs. Such existing methods include electrocoagulation, extraction, volatilization, hot gas or steam stripping, ion exchange, microbial degradation, membrane separation, solvent extraction, polymerization and many others (Tasic & Antonijevic, 2014).

Popular methods of phenol degradation that have continually gained interest are the adsorption technique and photocatalysis. Energy-saving and the vast opportunity to develop efficient adsorbents and photocatalytic semiconducting materials from abundant and cheap materials are major motivating factors that have favoured the interest in the two methods. Mainly, mixed solid oxides such as MgO-SiO2, Al2O3-SiO2, TiO2-SiO2, and ZrO2-SiO2 systems have long been studied due to their excellent catalytic activity resulting from the acid or basic properties (Itoh et al., 1974). Recently, the development of mixed metal oxides as adsorbents for wastewater treatment has attracted the attention of researchers due to their synergistic effect and enhanced adsorption capability (Chen et al., 2018).

More recently, Khan et al. (2021) employed (Fe-Mg) binary metal oxide to remove arsenic from contaminated water, and the adsorbent showed promising results regarding high arsenic uptake. In another study, Mustapha et al. (2021) prepared silver and titanium oxides-doped activated carbon as adsorbents to remove phenols from pharmaceutical wastewater. The reducing activity of whole extracts of Shea butter leaves on the nitrate salts of silver and titanium was illustrated towards the preparation of silver and titanium oxides, and an activated carbon doped with the oxides was found suitable for adsorptive removal of total phenols from pharmaceutical wastewater. Due to its environmentally benign principles and the potential to produce novel bespoke materials, green synthesis has proved to be one of the best processes for synthesizing metal oxide nanoparticles.

In the present study, the green synthesis method was utilized to develop a mixed oxide of MgO-TiO2 using leaves extract of Piliostigma thonningii and applied in an adsorption process (non-photocatalytic) towards the removal of phenol from process water sourced from a petroleum refinery.

# METHODOLOGY

#### Materials

Process wastewater was obtained from an indigenous Petroleum Refining and Petrochemical Company in Nigeria. Analytical grade magnesium nitrate hexahydrate (99%, Sigma Aldrich) and titanium nitrate tetrahydrate (99.9%, Sigma Aldrich) were used. Camel's foot leaf (Piliostigma Thonningii) was obtained from Ilorin, Nigeria. The leaves were sun-dried for 3 days, chopped into small pieces, and then a mortar and pestle were used to reduce them to powdery form. Dried powdered camel's foot leaves (4g) were introduced into the conical flask containing 100mL of distilled water. It was magnetically stirred (MS-H280-Pro digital magnetic hotplate stirrer) at 80°C for 50 min. Filtration of the extract yielded the filtrate that was used in the preparation of mixed oxide. Fourier transforms infrared spectrum of the extract from Piliostigma Thonningii were acquired using a Bruker Vertex 70 spectrometer (Bruker Optics, Billerica, MA, USA) to identify the presence of functional groups. Also, phenolic content in the refinery process water was estimated using the Folin-Ciocalteu method (Folin, 1927).

## Mixed oxide preparation and characterization

In a 400 mL conical flask, 5.75 g of titanium nitrate was dissolved in distilled water (15.63 mL) and stirred for 2 h to obtain 1M aqueous solution. In another flask, 15.9 g of magnesium nitrate was dissolved in distilled water (62 mL) and agitated for 2 h to obtain 1M aqueous solution. The two solutions were mixed, and 7.76 mL of leaf extract was added. It was centrifuged at 4000 rpm for 4 h and filtered. The filtrate was dried at 90 °C for 2 h and calcined at 500 °C for 3 h. Mixed oxide MgO-TiO2 was then stored in a sample bottle until use. Structural characterization of the mixed oxide was carried out using X-ray diffraction (Bruker AXS D8 Advance, USA), high-resolution scanning electron microscopy and Energy-dispersive X-ray spectroscopy (Zeiss Auriga, USA). The XRD pattern was acquired at room temperature (25°C) with Cu K $\alpha$  radiation ( $\lambda$ =1.5406 m). The spectra ranged from 15 to 80° at a step of 0.034°.

## Phenol degradation using mixed oxide MgO-TiO2

Batch adsorption experiments were carried out using Mixed Oxide (MgO-TiO2) to study the percentage of phenol removal. Adsorption conditions were varied for adsorbent dosage, contact time, and temperature, as shown in Table 1.

Variable	Dosage (g)	Contact time (min)	Temperature (°C)
(+)	0.1	80	50
(-)	0.02	10	35

#### **Table 1 Batch adsorption parameters**

A typical experiment added a measured quantity of the mixed oxide (0.02 g) to 50 mL of the refinery wastewater. This was followed by shaking the mixture in an orbital shaker at the desired temperature for a given period. Total phenol removal and the adsorption capacity were obtained from Equations (1) and (2), respectively;

% Removal = 
$$(C_0 - C_e) \times 100/C_0$$
.

Co and Ce are the initial concentration (mg/L) and the final concentration of phenol at equilibrium (mg/L), respectively.

(1)

$$q_e = \frac{(C_0 - C_e)V}{W} \tag{2}$$

Symbols represent adsorption capacity  $(q_e)$ , the volume of solution (V(L), and the mass of adsorbent (W(g). Three kinetic models were used to examine the experimental data acquired from the adsorption process to describe the mechanism controlling the adsorption process. These are presented in Equations (3) – (5), respectively, for pseudo-first order, pseudo-second order, and intra-particle diffusion models;

$$\log(q_e - q_t) = \log q_e - k_1 t / 2.303 \tag{3}$$

$$\frac{t}{a_t} = \frac{1}{k_2 a_a} + \frac{t}{a_a} \tag{4}$$

$$q_t = k_p t^{\frac{1}{2}} + C \tag{5}$$

Quantity of phenol adsorbed at a time,  $t(q_t)$ , and at equilibrium (mg/g)  $(q_e)$ , respectively, and  $k_1(l/min)$ ,  $k_p$ , and  $k_2$  (g/mg min) are the rate constants for the pseudo-first-order, diffusion of intra-particles and pseudo-second-order for the adsorption process. The constant C depicts the intra-particle diffusion, which indicates the boundary layer thickness. For this work, as presented in Equations (6) and (7), Langmuir and Freundlich's isotherms were respectively considered.

$$\frac{C_e}{q_e} = \frac{1}{bq_m} + \frac{C_e}{q_m} \tag{6a}$$

$$R_L = \frac{1}{1+bC_0} \tag{6b}$$

$$\log q_e = \log K_F + \frac{1}{n} \log C_e \tag{7}$$

In Equation (6a), *b* denotes the Langmuir constant, which is associated with the adsorptive energy (L/mg), while the maximum adsorption capacity (mg/g) is represented as  $q_m$ . The dimensionless equilibrium parameter,  $R_L$  is a crucial feature of the Langmuir isotherm that indicates the type of the isotherm to be either linear ( $R_L = 1$ ), favourable ( $0 < R_L < 1$ ), irreversible ( $R_L = 0$ ), or unfavourable ( $R_L > 1$ ), and  $C_0$  is the initial phenol concentration

mg/L. From Equation (7),  $K_F$  and n are the Freundlich constants that provide information about adsorption capacity and intensity, respectively.

The thermodynamics of the adsorption process of phenol onto MgO-TiO<sub>2</sub> mixed oxide was described using adsorption isotherms. The  $\Delta$ H and  $\Delta$ S were determined from the slope and intercept of the linear form of Van't Hoff's Equation (8) by plotting  $ln K_C$  against  $^{1}/_{T}$ . The change in Gibbs free energy  $\Delta$ G was determined at different temperatures from equation (9).

$$lnK_C = \frac{\Delta S}{R} - \frac{\Delta H}{RT}$$
(8)

$$\Delta G = (\Delta H - T\Delta S) \tag{9}$$

In the equations, R is the universal gas constant, T is the absolute temperature in Kelvin, and  $K_C$  Is the equilibrium constant representing the ratio of adsorption capacity to the amount of adsorbate in the solution at equilibrium ( $K_C = Q_e/C_e$ ).

### **RESULTS AND DISCUSSION**

Fourier transform infrared spectrum of Piliostigma thonningii leaves extract was obtained (Figure not shown). In the spectrum, a peak due to N-H stretching bond or carboxylic acid (COOH) and aliphatic hydroxyl (OH) groups was observed at 3480 cm-1. The wavenumber 707 cm-1 is due to C-S stretching bond, alkyl halides, or the double bond -CH=CH-. Aromatic rings, carbonyl group (C=O) vibration or ethylenic double bond (C=C) were observed at 1634 cm-1. The peak due to the triple bond C  $\equiv$  C stretching bond at 2052 cm-1 was also evident. The presence of amine groups in the Piliostigma thonningii leaves extract, as observed in the FTIR result, indicates the leaves extract's suitability as a reducing agent for the biosynthesis of MgO-TiO2 mixed oxide. Also, the existence of diverse bioactive molecules in the leaves extract of Piliostigma Thonningii will serve to reduce, cap/functionalize, or stabilize the mixed metal oxide nanoparticles in the course of synthesis. The amount of total phenols in the petroleum refinery process water was reported as 19.961 mg/L

The X-ray diffraction pattern of the prepared MgO-TiO2 mixed oxide is presented in Figure 1. The XRD peaks are mainly due to rutile and anatase phases of titanium oxide (rutile: JCPDS card no. 00-021-1276) and (anatase: JCPDS card no. 00-021-1272). Peaks due to magnesium oxide were not revealed, perhaps because they are relatively less crystalline than the anatase and rutile polymorphs of TiO2. Nonetheless, the presence of MgO has been supported by qualitative and quantitative EDX elemental compositions and high-resolution scanning electron microscopy images.



Figure 1 The XRD pattern of mixed oxide MgO-TiO<sub>2</sub>

The EDX elemental analysis showed that titanium and magnesium oxides were present in the sample, as shown in Figure 2. In addition to Ti, Mg and O from the mixed oxide, other elements found in the mixture are: C, Al, and Si, which were introduced by the leaves extract used in mixed oxide preparation. It was revealed in the EDX elemental composition that the elements were present in atomic% as C(8.23), O(70.63), Mg(0.87), Al(1.01), Si(0.65), and Ti(18.6). Analysis of the XRD and EDX results imply that the formation of titanium and magnesium oxides from their corresponding nitrate salts was effective.



Figure 2 The EDX result of the MgO-TiO<sub>2</sub> mixed oxide

The rutile (tetrahedral, tetragonal) and anatase (octahedral) structures of the titanium oxide polymorphs present in the MgO-TiO2 mixed oxide are confirmed by the HRSEM morphologies presented in Fig. 3(a) - (d). Calcination would have caused the phase transformation of the initially formed anatase into the rutile phase. Additional smaller structures appear on the surfaces of the well-defined crystalline titanium oxides, possibly those of magnesium oxide. In Fig. 3(b), micropores can be identified in the nanoparticles, a property indicating that the mixed oxide would possess sufficient active sites for surface adsorption. The BET surface area of the synthesized MgO-TiO2 nanoparticles was 215.50 m2/g. A larger surface area provides more surface active sites for the adsorption of phenols from the refinery wastewater.



**Figure 3** HRSEM Images of the MgO-TiO2 mixed oxide nanoparticle (adsorbent) with rutile TiO2 indicated (a), anatase TiO2 showed (b), and images in (a),(b) repeated at a different magnification (c),(d).

In the phenol adsorption studies using the mixed oxide, contact time, adsorption temperature, and the adsorbent loading had notable influence towards the percentage removal of phenol, as revealed in Fig. 4(a) - (c)). The optimal (most favourable) contact time was reached after 70 minutes, after which the efficiency declined (Fig. 4a). The initial high rate of phenol uptake had been related to the greater vacancy on the active adsorption sites (mixed oxide surfaces). It was observed that the phenol removal rate declined gradually after reaching the optimum at 70 minutes because most of the available sites were occupied. It is shown in Fig. 4(b) that the percentage of phenol removal was best at 35 °C, which occurred at the optimum contact time of 70 minutes, and adsorbent dosage of 0.02 g. Fig. 4(c) presents the relationship between percentage phenol removal and adsorbent loading (dosage). An optimum point in percentage phenol removal was attained with 0.04 g of MgO-TiO2 mixed oxide, occurring at 35 °C and time 70 minutes. This condition resulted in 99.5 % removal of phenol. An additional dose of adsorbent resulted in a saturated aqueous mixture and could therefore block active adsorption sites, thereby causing a reduction in phenol removal due to insufficient sites.



**Figure 4(a)** Time-dependent phenol removal by the mixed oxide (b) Temperature-dependent phenol removal by the mixed oxide (c) Adsorbent dosage-dependent phenol removal by the mixed oxide

As shown in Fig. 5 (a) and (b) are the respective graphs of the kinetic models. Table 2 lists the pseudo-first order and pseudo-second order parameters as determined. The model of pseudo-first order kinetic better depicted the adsorptive phenol removal by the MgO-TiO2 mixed oxide, and it was found that both were calculated.  $q_e$  and experimental  $q_e$  agree and followed the pseudo-first-order model, and the (R2) value was much closer to one (1.0) than the pseudo-second-order kinetic model. Plotting of  $q_t$  against t1/2 in Fig. 5(c) showed a linear graph due to the adsorption process's intra-particle diffusion. Such a linear graph that tends to deviate from the origin indicates that the rate-controlling step is not only controlled by the intra-particle diffusion but may also result from some extent of boundary layers (Angin, 2014).



**Figure 5** Fitting the phenol removal by MgO-TiO<sub>2</sub> mixed oxide to (a) pseudo-first-order kinetics (b) pseudo-second-order kinetics (c) intra-particle diffusion.

Pseudo First Order		Pseudo Second order		Diffusion of intra-particles			$q_e(Exp)$		
$R^2$	<i>K</i> <sub>1</sub>	$q_e(\text{Cal})$	$R^2$	<i>K</i> <sub>2</sub>	$q_e(\text{Cal})$	$R^2$	K <sub>P</sub>	С	
	$min^{-1}$	mg/g		g/mg.min	mg/g		$mg/g.min^{\frac{-1}{2}}$	mg/g	mg/g
0.7796	0.03086	53.80	0.6557	0.000292	67.11	0.861	0.151	1.796	47.03

Table 2 Kinetics parameters for the phenol removal by the mixed oxide

The plot in Fig. 6(a) showed that the Langmuir isotherm model fitted well to the experimental data with R-squares values of 1.0 when compared to the Freundlich isotherm with an R-square value of 0.9664. This means that the uptake process took place on a homogenous surface by a monolayer adsorption mechanism; all sites were occupied at once, and the binding strength is attributed to the phenol concentration at equilibrium. The ultimate adsorption capacity was 48.077 mg/g, and the RL obtained was 1.008, indicating a linear model for the adsorption process. The negative value of 'n' from the Freundlich isotherm plot in Fig. 6(b) suggests a chemical interface and an unfavourable adsorption route of phenol on the adsorbent. Also, the large value of Kf indicates a high adsorption capacity (Vasudevan, 2014). However, the adsorption process was well fitted into the Langmuir isotherm (Fig. 6a). Table 3 summarises the results.



**Figure 6 (a)** Langmuir Isotherm for phenol adsorption onto MgO-TiO<sub>2</sub> (b) Freundlich Isotherm for phenol adsorption onto MgO-TiO<sub>2</sub>

	Langm	Langmuir constants			Freundlich constants		
$R_L$	$q_m$ (mg/g)	b(l/mg)	<i>R</i> <sup>2</sup>	n	$K_f(\text{mg/g})$	<i>R</i> <sup>2</sup>	
1.00	48.077	0.4069	1.0	-93.4577	47.8189	0.9664	

Table 3 Langmuir and Freundlich constants for the adsorption of phenol onto MgO-TiO<sub>2</sub>

The thermodynamic plot for the phenol adsorption in refinery process wastewater using the MgO-TiO2 mixed oxide is shown in Figure 7. Enthalpy was found to be  $\Delta H = -16.36195$  KJ/mol, which means that the adsorption of phenol on MgO-TiO2 is an exothermic reaction. The entropy  $\Delta S = -53.05$  J/mol K suggests less randomness at the solid-solution interface and that adsorption does not require much energy. Gibb's free energy values were -0.023 kJ/mol, 0.240 kJ/mol, 0.510 kJ/mol and 0.770 kJ/mol at temperatures 308, 313, 318 and 323 K, respectively. The negative sign of Gibb's free energy at the optimum temperature indicates spontaneous adsorption, while the positive sign of Gibb's free energy above the optimum temperature indicates non-spontaneous adsorption (Djebbar et al., 2012). Values are presented in Table 4.



Figure 7 Thermodynamic curves for the phenol adsorption using the mixed oxide

		308K	313 K	318 K	323 K
$\Delta H$ (kJ/mol)	-16.36195	-	-	-	-
$\Delta S (kJ/mol)$	-0.0531	-	-	-	-
$\Delta G (kJ/mol)$		- 0.023	+ 0.240	+ 0.510	+ 0.770

Table 4 Thermodynamic parameters for phenol adsorption using the mixed oxide

# CONCLUSION

The synthesized mixed oxide nanoparticles of MgO-TiO2 were found suitable for adsorptive phenol removal from refinery process wastewater. The reducing activity of the whole extract of Piliostigma thonningii on the nitrates of magnesium and titanium was illustrated towards the preparation of magnesium and titanium oxides. With an initial phenols concentration of 19.96 mg/L in the raw refinery wastewater, a maximum percentage removal of 99.50% was achieved using a MgO-TiO2 dosage of 0.04 g, contact time of 70 min and temperature of 35 oC. Langmuir isotherm and pseudo-first-order kinetic model defined the experimental adsorption data from the equilibrium and kinetic studies. It was found from the intra-particle diffusion model that the adsorption rate was not controlled only by intra-particles but was also controlled by exterior mass transfer at the early stages of the process. It was also established that the adsorption process was spontaneous and exothermic at the optimum temperature.

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