An investigation on supercapacitors applications with module designing and testing

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ABSTRACT

Supercapacitors have high power density and some advantages than other storage devices. Therefore, the applications of supercapacitors and investigations to develop their materials and chemistry are increasing every day. Also, the engineering and energy storage applications of supercapacitors are being continuously researched. The structural properties of supercapacitors and their technical applications based on an extensive literature review are given in this paper firstly. Then, requirements for module design for supercapacitors are revealed, and module design is carried out and set up. The supercapacitor module design is performed in MATLAB/Simulink software, and the simulation results are obtained for the charge and discharge conditions. Measurements are performed at various load conditions, and results are compared with simulation results and rated with supercapacitor manufacturers' datasheets. The power storage capacity of supercapacitor modules and discharging as a function of time is obtained experimentally. These results give us information about the power density of supercapacitors for different loads, and how long and how much the current can be given. This study can be considered as a preliminary study on supercapacitors to be used in power electronics, renewable energy, and electric vehicle applications, instead of conventional energy storage techniques. The detailed review of the literature and the obtained data in the present paper shed light on further studies to be performed in the field.

Keywords: Current storage technologies; Supercapacitors applications; Supercapacitor module design; Modelling of supercapacitor; Charge and discharge tests of supercapacitors.

INTRODUCTION

Supercapacitors (SCs) were used for many years in wind turbines, mobile base stations, electronic devices, and different industrial practices (Libich et al., 2018, Kuperman et al., 2012, Bottu et al., 2012). On the other hand, they have started to be used in uninterruptible power supplies, electric vehicles, and various power electronics applications thanks to their superiority over the lead-acid batteries recently (Eroğlu, 2010, Schneuwly, 2015, Lee, 2015). In recent years, the SCs are used as energy storage devices for voltage stability in renewable and hybrid energy storage systems to regulate the source and grid side (Rawat et al., 2019, Shuai et al., 2020, Şahin et al., 2020).

When the superiorities of supercapacitors are observed firstly, it can be realized that they can store the same amount of power in a smaller volume compared to a battery (Eroğlu, 2010, Ortúzar, 2005). Supercapacitors get less affected by impulse currents, and they can decrease these impulse currents. The most important reason for that is

their ability to make a fast charge and discharge. Batteries get worn out in these processes. Whereas SCs can be charged/discharged for hundreds of thousands of times, batteries can be charged/discharged for a thousand times at the most, and they lose their properties with time (Zhang et al., 2018). Another specification of SCs is that they have very low internal resistance and much higher volume (Sahin et al., 2020). While SCs can be charged/discharged within a range from zero volting up to the allowed value, it is difficult to do the same with the batteries. Batteries get damaged if they are overcharged or overdischarged (Sahin et al., 2021). Therefore, a wide range of bus voltage can be selected. The charge level of SCs is directly related to the capacitor and voltage value, and it can easily be detected, but it is difficult to detect the level of charge in batteries. Again, the operation temperature range of supercapacitors is quite wide (Kreczanik et al., 2013, Headquarter, 2013). This level can decrease to -10 °C -40 °C range in supercapacitors (URL 1, 2020, URL 2, 2020, Prummer et al., 2015). Also, temperature, voltage, and currents are the main parameters that accelerate the aging of SC (Kreczanik et al., 2013).

When the literature on SCs is considered, it can be seen that these studies can be divided into three groups, and it would be more appropriate to deal with them in groups. The first group of studies mainly describes the characteristics of SCs and testing of these characteristics. The second group of studies is based on the applications of supercapacitors in automotive, hybrid vehicles, and the transportation industries. The third group is those who are dedicated to renewable power sources and the network-related systems and their power electronics applications.

A. Basics and Characteristic Properties of Super Capacitors

The studies conducted on the basics and characteristic properties of supercapacitors were considered here. In one of these studies, temperature and dynamic programs of supercapacitors were investigated, and their efficiency changes were analyzed (Hartmut, 2006). It was emphasized that a cooler unit was necessary for module designs. In another study conducted on the characteristics and modelling of supercapacitors, this method was analyzed for utilization of sudden power need, and impulse, frequency, and voltage rates were determined in the first place for the hybrid electric vehicles (Lajnef et al., 2007). The dynamic behavior of supercapacitors was the focus of interest initially. Then, a dynamic model was created for supercapacitors, and the results obtained were compared for different parameters. A study conducted on capacity and leakage current balancing for supercapacitors focused on the voltage imbalance observed in supercapacitor modules for different capacity values and different leakage resistance (Latkovskis et al., 2012). The study offered a solution that decreases the imbalance of cell voltages and increases the storing efficiency of supercapacitor modules utilizing capacitor balance and passive resistance voltage balance. The efficiency of the method was theoretically proven and tested on eight capacitor modules. The theoretical and experimental results obtained show that the capacitance balancing in parallel/series SC connection significantly improves the effective energy capacity of the SC bank (Latkovskis et al., 2012). In another study that was conducted to test the lifetimes of supercapacitors when used for long periods, a MATLAB/Simulink software installed computer-controlled testing apparatus was designed to check whether the lifetimes specified by the manufacturers were true or not (Murray et al., 2015). This study also defined the temperature changes of supercapacitors and their impact on their lifetime. Supercapacitors are tested in normal operating conditions for two years and up to ten million cycles. It was observed that supercapacitors operated within the specified tolerance range without any trouble. These results confirmed the manufacturer's catalogs and showed that supercapacitors could be used in applications that require long lifetimes. A virtual laboratory is performed to test the characteristics of supercapacitors and batteries, applications of supercapacitors, and battery energy storage components (Freeman et al., 2013). The setup allowed the users to reveal the charging/discharging capacities of different types of batteries and supercapacitors. The study brought new ideas and enabled observation of the number of energy stores. Some other studies about the characteristics of supercapacitors will be mentioned in the modelling section.

B. The Electrical Vehicle Applications of Supercapacitors

The studies conducted on the electrical vehicle applications of supercapacitors were also reviewed. In a study conducted by Cyrus et al. on electrical vehicle applications, the automotive applications of supercapacitors were reviewed, and the supercapacitor module was projected to be connected in parallel with the output load (Cyrus et al., 2006). Characteristics of different supercapacitors were studied and compared, their charging/discharging test graphics were drawn, and several comparisons were made. Subsequently, potential applications in the automotive industry were identified, and a consensus requirement specification was drawn as a development guide for the industry (Cyrus et al., 2006). In another study conducted by Steiner et al., supercapacitor supported energy storing systems for tramway vehicles were addressed (Steiner et al., 2007). This system, which had been in use since 2003, was observed to provide around 30% energy saving. It also had other benefits including decreasing the peak flow need, enabling the trains to go hundreds of meters without the need for energy, and enabling cost-free charging stations at stops. With the help of the latest technologies, researchers of today are trying to develop systems that can store 600 kW energy in 16 seconds at every stop (Matthias et al. 2015). Some other studies conducted by Paseran et al. (2005), Anstrom et al. (2005), and Farzad et al. (2011) dealt with the systems where batteries and supercapacitors were connected in parallel for the charging systems of the electrical vehicles. In the first study, battery and supercapacitor properties needed for the electrical vehicles were determined, and the potential results of their coutilization were revealed out. The results were tested with an eight-cell supercapacitor module (Paseran et al., 2005). In the other study, simulation studies and field tests were conducted for supercapacitor and battery charge systems of hybrid and electric vehicles. It was observed at the end of several tests that supercapacitors enabled significant improvements in peak flow as a spare source for batteries (Anstrom et al., 2005). The third study dealt with the modelling of a charge station for dual direction DC/DC converter and hybrid electric vehicles and determination of its benefits. That study aimed to lower the costs of the electric vehicle charge stations and to show the increase in high energy density and efficiency of the hybrid system by making use of Li-ion battery supercapacitor and two DC/DC converters. The result revealed that the hybrid energy storing system performed better than batteries and supercapacitors in the procurement of high energy and energy density (Farzad et al., 2011). Various energy storage systems (ESS) specifications meeting in the electric vehicles 42V Start-Stop minimum requirements are shown in Table 1.

Description	Number of Modules	Parallel Strings	Nominal Voltage	10S Power	2S Power	Usable Energy	Mass	Cost	Volume
Units	-	-	V	kW	kW	Wh	kg	\$	L
PbA only	3	1	37.89	7.8	7.85	256.7	33.0	330	11.6
UC only (2600 F)	20	1	39.5	14	54	35.0	14.2	600	21.7
Li-ion (6Ah)	22	2	40.93	12.1	12.1	156.7	8.3	440	6.6
NiMH (6.5 Ah)	10	2	39.78	7	7.8	125.0	10.0	400	8.8
3 PbA + 7 UC (PbA@HV)	(3+7)	n/a	37.89	12.5	27	271.7	46.4	847	22.0

Tablo 1. Various ESS specifications meeting the 42V start-stop (Paseran et al., 2005).

The objective of another Ph.D. thesis research is to develop suitable models to simulate and analyze Electrical Vehicle (EV) power-trains to identify and improve some of the deficiencies of EVs and investigate new system architectures. Multiple energy source systems are modelled and studied in the form of an energy-dense ZEBRA battery technology connected in parallel with a power-dense supercapacitor system. This study offers a suitable model for different energy sources and then optimizes the vehicle energy storage combination to realize its full potential (Jarushi, 2010). A book study about environmental impact and history of a modern vehicle with fundamentals is given first. HEVs and their energy storage system with supercapacitors are given in this book. The future of supercapacitors, basic principles, performance, and supercapacitor technologies are investigated in more detail in the chapters of this book (Ehsani et al., 2018).

C. Other Utilization Areas of Supercapacitors

Other utilization areas of supercapacitors such as smart networks, renewable energy, and power electronics were also reviewed in this chapter. Firstly, the energy sources modelling of hybrid electrical vehicles given in the study conducted by Van Mierlo et al. (2004) dealt with the fuel cells, battery, supercapacitor, and flywheel motor described. The advantages and properties and the equivalent model of the supercapacitor component were presented. Nevertheless, this study was not comprehensive, and it did not sufficiently investigate the supercapacitor components. The study conducted by Miller et al. (2010) focused on supercapacitor and battery as a hybrid energy-storing model. The type of power electronics converter setup needed for the provision of such a hybrid system, and the necessary properties were dealt with. Simulations were made for utilization in different converter structures and electric vehicles, and the results were compared. In another study, the maximum charge condition of the supercapacitor of the switched rectifier for one circuit was studied (Kleas, 2005). An algorithm that regulated the duty cycle of the DC/DC Buck-Boost Converter was designed to enable the synchronous generator to work at the maximum power point when being charged with supercapacitor, and simulations were made. In another study conducted by Daboussi et al. (2007), a Lithium-ion-Supercapacitor hybrid energy module that included some simulations and experimental results was presented. An optimized Li-ion/ultra-capacitor Hybrid Energy Module (HEM) is presented in this paper to determine the optimum utilization of ultra-capacitors in hybrid vehicle and space applications where high power density and high energy density are required. In another study conducted by Wei et al. (2011), DC micro-networks were emphasized as a candidate that would fulfill the needs of the smart networks of the future, and it was stated that the most significant issue here was to go beyond the ordinary production and to work with maximum efficiency by making using of renewable energy and storing and by minimizing the cost. The two load sharing methods as the subsequent and parallel are presented in DC/DC converters for multisource input in this article. Experimental and simulation studies that showed the impact of this new method are given (Wei et al., 2011). Finally, this study presents the reduction in battery stresses by using SCs in a 500 kVA rated UPS. The authors investigate the optimal supercapacitors, battery combination versus the SCs cost. The SCs and battery models developed using MATLAB/Simulink are presented and validated. The architecture and simulation of the designed system that combines the SCs and battery were shown. The supercapacitors were used as high power storage devices to smooth the peak power applied to the battery (Lahyani et al., 2012; Sahin et al., 2021).

In the conclusion of this chapter, the utilization of supercapacitors seems quite useful considering the superiorities of supercapacitors. On the other hand, there are also some disadvantages. First of all, the SCs cost too much; however, new technologies are being researched to decrease the prices of these products by the manufacturers and scientists. But this can be compensated by its long-term charging/discharging property. Another disadvantage is that supercapacitors have a higher power density than batteries, yet a lower energy density (Headquarter, 2013). The performance analyses of lead-acid, lithium-ion batteries, and supercapacitors are compared in Table 2 (Jing et al., 2016; URL 3, 2020, Glavin et al., 2008; Manandhar et al., 2017).

Parameters	Lead-acid Battery	Lithium-ion Battery	Supercapacitor
The specific energy density (Wh/kg)	10-100	150-200	1-10
Specific power density (W/kg)	<1000	<2000	<10000
Cycle life (cycles)	1000	5000	>500000
Charge discharge efficiency	70-85 %	99%	85-98 %
Fast charge time	1-5 hours	0.5-3 hours	0.3-30 sec
Discharge time	0.3-3 hours	0.3-3 hours	0.3-30 sec
Calendar life (year)	5-15	10-20	20
Cost	Low	High	Medium

Table 2. Performance analyses of lead-acid, lithium-ion batteries, and supercapacitors.

Considering the advantages and disadvantages of SC, it seems the most rational thing to install a system in an appropriate voltage and power value where the two systems are used together (Libich et al., 2018, Kuperman et al., 2012, Schneuwly, 2015, Lahyani et al., 2012).

In this papar, firstly, a detailed literature review is made about SC and their applications. Within this framework, supercapacitor values suitable for the established system power that would ensure the necessary bus voltage were selected, and these capacities were used to design a supercapacitor module that would meet the need in different voltages (12 V, 24 V, 48 V). Different load conditions of supercapacitors were considered for these operating conditions, and the charging-discharging tests were conducted. The supercapacitor modules were tested, compared, and rated with the alone supercapacitors and MATLAB/Simulink simulation results.

METHODS AND MATERIAL

1.1 The Structure and Properties of Supercapacitors

Today, supercapacitors are produced in different properties by several manufacturers (URL 1, 2020, URL 2, 2020). They are produced by different voltage and capacity ranges for different applications. Also, they include coin type, winding type, combined type, module, high-temperature SC, and hybrid capacitor (URL 5, 2020, URL 6, 2020). Market research was made, and Maxwell brand BCAP0310 model 310 F and 2.7 V charging voltage supercapacitors that could be mounted on the printed circuit were selected for the design. Looking at the catalog data, it is observed that these capacities have 2.2 m Ω ESR_{DC} resistance, and they can be supplied by 2.85 V voltage, and the continuous current is 25 A for 15 °C. The peak current of this SCs for one second is 250 A, the maximum leakage current is 0.45 mA, and it can preserve its voltage for 72 hours in normal conditions. Furthermore, it is observed to be able to work from -40 to +70 °C. Each of them has 61.5 mm in height and 3.3 cm in diameter (URL 1, 2020).

The image of the SCs used for module design and the electrical equivalent circuit model are given in Figure 1. The series resistance (R_s) here represents the equivalent series resistance (ESR), whereas the parallel resistance (R_p) represents the resistance estimated according to the leakage currents, and the capacitance (C_{UC}) represents the total capacitance of SCs.



Figure 1. The image of used supercapacitor (a), equivalent circuit model (b) (URL 1, 2020).

The above parameters mentioned in the catalog data can be used to calculate the values in the following equations (URL 1, 2013). The maximum instant current in a second and the other necessary values can be calculated by making use of the Equations 1 to 4.

Maximum Peak Current (1sec) =
$$\frac{1/2.C.V}{C.ESR_{DC}+1}$$
 (1)

$$P_{\text{max}} \left(\text{Specific Power} \right) = \frac{V^2}{4.\text{ESR}_{\text{DC}}.\text{mass}}$$
(2)

$$E_{\text{max}} \text{ (Specific Energy)} = \frac{\frac{1}{2} \cdot C \cdot V^2}{3,600.\text{mass}}$$
(3)

$$E_{s} \text{ (Storable Energy)} = \frac{1/2 \cdot C \cdot V^{2}}{3,600}$$
(4)

1.2 Modelling and Simulation of the Supercapacitor Module

There are several studies in the literature where chemical, mathematical, and electrical stimulation of supercapacitors were investigated (Johansson et al. 2008, Michalczuk et al., 2015, Faranda et al., 2007, Shah et al., 2012, Buller et al., 2002, Cheng et al., 2010, Islam et al., 2010, Zubieta et al., 2000). The module simulation was based on the most comprehensive of these studies, which also included the module structure and its mathematical equation simulation (Seim, 2011, Oldham, 2008, Riley, 2011, Monzer et al., 2010). The chemical structure of SC modules and the chemical and electrical reactions during charging are illustrated in Figure 2. As being different from other condensers, the separators were utilized, and a structurally different dual-layer capacitor is seen (Seim, 2011). Nanomaterials are started to be used in SC design today, and the preparation of nanoporous iron oxide/carbon composites provides a highly accessible path for the diffusion of electrolyte ions (Azhar et al., 2019).



Figure 2. Chemical structure of supercapacitor for the uncharged and charged states (Azhar et al., 2019).

In a study, the dual-layer capacitor model was developed for two different structures (Oldham, 2008). According to this model, the potential difference between the metal-electrolyte solutions for electrolyte solution structure can be written as in Equation 5. Descriptions regarding the variables valid for Equations 5 to 9 are given in Table 3.

$$V = \frac{q.d}{\varepsilon} + \frac{2RT}{F} \operatorname{arsinh}\left\{\frac{q}{\sqrt{8RT\varepsilon c}}\right\}$$
(5)

Based on this mathematical model, the total potential difference belonging to the block structure obtained through a serial and parallel connection of supercapacitors can be written as in Equation 6.

$$V_T = \frac{N_s Q_T d}{N_p N_e \varepsilon \varepsilon_0 A_i} + \frac{2N_e N_s RT}{F} \operatorname{arsinh} \left\{ \frac{Q_T}{\sqrt{8RT \varepsilon \varepsilon_0 c}} \right\}$$
(6)

The current of a supercapacitor is can be written as in Equation 7.

$$i = i_{\rm sc} \cdot \left(1 - u(t)\right) + i_{\rm self_dis} \cdot u(t) \tag{7}$$

Based on these equations, the equivalent circuit model belonging to the most commonly used supercapacitor block is given in Figure 3 (a) (Riley, 2011, URL 3, 2020).

Equation 8 is observed between the super capacitor's total load and current for $i_{sc}=0$. The $I_{self_{dis}}$ current is given as in Equation 9. The α value in this equation is a fixed value, and it is related to the change observed in the voltage rate of supercapacitor in time.

$$Q_T = \int \dot{\mathbf{I}}_{\text{SC}} dt \text{ and } Q_T = \int \dot{\mathbf{i}}_{\text{self}_\text{dis}} dt \text{ (for } \dot{\mathbf{i}}_{\text{sc}} = 0 \text{)}$$
(8)

$$i_{\text{self}_\text{dis}} = \frac{c_T \alpha}{1 + s_{R_{SC}} c_T} \tag{9}$$

Variable	Description	Variable	Description
A_{I}	Surface area between the electrode and electrolyte (m ²)	Rsc	Total resistance
С	Molar condensation	Ne	Electrode plates number
F	Faraday constant	NA	Avogadro number constant
isc	Supercapacitor current (A)	Np	Parallel supercapacitors numbers
$V_{\rm SC}$	Supercapacitor potential (V)	Ns	Series supercapacitor numbers
Ст	Total capacity	QT	Electrical Capacity (C)
R	Ideal gas constant	d	Molecular permeability
Т	Study temperature (K)	Е, Ео	Material's and air permeability

Table 3. Descriptions for the variables used in the supercapacitor model.

The supercapacitor MATLAB/Simulink functional model with the charge and discharge setup is given in Figure 3 (b). The simulation setup is designed with a similar experimental setup to be compared to the simulation and experimental results. The simulation results for a single capacitor charge/discharge conditions current, voltage, and power curves for different load and ESR conditions (0 to 1 Ω) are given in Figure 4 (a–d). The simulation results for five series-connected capacitor single module charge-discharge current, voltage, and power curves for 1 Ω load and ESR conditions are given in Figure 4 (e). The simulation results will be compared with the experimental results in the next parts.





Figure 3. (a) Equivalent model for supercapacitor block. (b) The SCs MATLAB/Simulink model with the charge and discharge setup.





Figure 4. For a single capacitor charge/discharge conditions current, voltage, and power curves for 1 Ω (a), 0.5 Ω (b), 0.25 Ω (c), 0 Ω (only for ESR) (d) resistances, (e) for a single module charge/discharge current, voltage, and power curves for 1 Ω load.

2.3 Design of Supercapacitor Module

Supercapacitors do not provide a sufficient amount of constant current alone and cannot reach the desired level of voltage. So, it was required to design a module to obtain the desired current and voltage values by connecting supercapacitors in series and parallel. Therefore, a module with a maximum voltage capacity of 5 x 2.7=13.5 V was created by connecting five pieces of 310 F, 2.7 V supercapacitor in series. These modules were developed to design supercapacitor modules by using the twenty pieces of supercapacitors. That could be connected in parallel to 12 V, 24 V, and 48 V bus voltages through different types of connections. While high levels of voltage are obtained by connecting the modules in series, high levels of current are obtained by connecting them in parallel. The system intended for the utilization of the module with 24 V and 12 V bus voltages seemed appropriate to connect the modules in doubles as series and parallel. When all the modules are connected in series, utilization in a 48 V system can be possible. The circuit model and the printed circuit diagram, which are designed in Eagle software for this connection, are shown in Figure 5.



Figure 5. Circuit of supercapacitor module (a), printed circuit board wiring diagram (b).

RESULTS AND DISCUSSIONS

As the catalog data of the SCs used did not give the charge-discharge curves, and to get more information about SCs, charge/discharge tests needed to be performed. These tests were also used to control the effect of different load conditions and to confirm their suitability within the module structures for the system to be established. The experimental setup given in Figure 6 was developed for this purpose.



Figure 6. Circuit diagram for testing supercapacitors (a), experimental setup (b).

The charge and discharge tests of a single supercapacitor for 2.85 V charge voltage were conducted initially for different load conditions to find out the instant current, charging time, and the instant power values of the supercapacitor in the experimental setup. The data obtained at the end of measurements were used to get the current, voltage, and instant power graphics given in Figures 7 and 8 for charge-discharge conditions. In the measurements given in Figure 7, supercapacitors in different load conditions were charged up to 2.85 V levels, which is the maximum level allowed. In these conditions, the charge time gets longer for high series resistance, and it gets shorter for small resistance. Whereas it takes 20 minutes for 1 Ω series resistance, it takes as short as 4 minutes in short circuit condition.

If we make a time constant analysis for these capacitors, the time constant can be defined as $\tau=R.C$, and it can be calculated for 1 Ω load and 310 F capacitors theoretically as $\tau=1 \times 310=310$ seconds. On the other hand, the time constant can be calculated from Figure 7 (a–d) experimentally. If we find the value V_0/e and mark it on the graphics, the cross graphic time value shows the experimental time constant of the capacitors. The values are seen suitable with the theoretical results with a little different depending on the capacitor's input resistance, cable, and measurement devices resistances.



Figure 7. For a single capacitor and different resistance charge voltage (a), and current (b), discharge voltage (c), and discharge current (d).

In the measurements given in Figure 8 (a-b), supercapacitors were charged at 2.85 V level and discharged at different load conditions. In these conditions, it is observed that whereas the time gets longer for high series resistance, it gets shorter for low resistance. Whereas it takes 20 minutes for 1 Ω series resistance, it takes even shorter than 4 minutes in short circuit condition.

The results given in Figure 8 (a-b) include the instant power values estimated by using the constant current and voltages that emerge during charge and discharge of supercapacitors up to 2.85 V level. In these conditions, whereas the time gets longer for high series resistance, it gets shorter for low resistance. Another issue seen in these graphs is that when a certain level of voltage is reached in instant charge condition, the maximum power is drawn. During the discharge condition, the SC voltage will be at the highest level and give the maximum current. Maximum instant power is drawn at first, and then it has seen an exponential decrease in time. It was observed, in a short circuit condition, that a single supercapacitor could emit 60 W instant power. 80% of this power is consumed in the first 30 seconds, and 98% of it is consumed in the first 60 seconds. While the power drawn gets decreased in different load conditions, the discharge time gets longer. This is an advantage during charging and instant power drawing.

In the further stage of the experimental study, charge and discharge tests of a single supercapacitor module, which consists of five series SCs for 15 V charge, were conducted for 1 Ω load condition to reveal the constant current, charging time, and the instant power values. The data obtained at the end of the measurements were used to get the current, voltage, and instant power graphics given in Figure 8 (c-d) for charge-discharge conditions.



Figure 8. For a single capacitor and different resistance conditions charge (a), and discharge (b) instant power. For a single module and charge (c), discharge (d) conditions current, voltage, and power curves.

The experimental results in Figure 8 (c-d) show the observation to see the charge and discharge conditions of the module obtained when connecting five pieces of SCs in series by using 1 Ω series resistance. The maximum current of 10 A and 50 W power was drawn in charge condition. The supercapacitor got fully charged in six minutes. In discharge condition, 11 A of current was drawn for 1 Ω load resistance, and initially, 160 W instant power was consumed. 30% of this power was consumed in the first minute, and the power consumed in two minutes decreased lower than 10% of the initial value. As our power supplies and measurement tools did not allow us to reach higher current and voltage levels, measurements at lower resistance could not be performed. The measurements are observed to be in conformity with the catalog data and to be able to meet the need.

Considering that the voltage and current capacities will almost double when two series and two parallel module connections are made for the same load conditions, we can say that 44 A of instant power can be drawn for 24 V bus voltage. In this case, it would be possible to drive around 1100 W instant power from the supercapacitor module designed. This would significantly decrease the constant voltage drops and the aging that might happen in batteries. This study will be further tested through other studies by connecting the supercapacitor module in parallel with the batteries. It is also possible to draw shorter-term instant currents for lower load resistances. Detailed results of the measurements are presented in the table in Appendix 1.

The experimental results show that the SCs have more superiority than conventional capacitors and other storage devices in many ways. It is possible to obtain instantaneous high currents without voltage drops as shown in the results. The module structure strengthens this demand more efficiently. This cycle can be repeated thousands of times without any deformation in SCs.

At last, a comparison time of experimental and simulation results for charge and discharge of SCs for different resistors is given in Table 4. The table shows that the experimental and simulation results are suitable for each other with a neglected small error of less than 0.01. The inconsistency between some power results depends on the multiplication of values, because of the square of error reduces the values. The table shows that, for big value loads and low power consumption, the SCs can give more than 1000 seconds of energy. These values are enough for instantaneous power generation and consumption. These values can be rated depending on the high power generation and consumption ratio. This is possible in the designed module with increasing the capacitor values and connecting them series and parallel.

Resist	ance Value	1	Ω	0.4	5Ω	0.25	5Ω	0	Ω	1 Ω (N	Iodule)
Charge Sit	/ Discharge tuation	Charge	Discharge								
Voltage	Simulation	1200	1200	900	900	840	840	240	240	420	420
Time (second)	Experiment	1200	1200	900	900	840	840	240	240	420	420
Current	Simulation	1200	1200	900	900	840	840	240	240	420	420
Time (second)	Experiment	1200	1200	900	900	840	840	240	240	420	420
Power	Simulation	1200	1200	900	900	840	720	240	150	420	300
(second)	Experiment	1200	1200	900	900	840	720	240	150	420	300

Table 4. Comparison timetable of experimental and simulation results.

CONCLUSION

The detailed literature survey revealed the benefits of supercapacitors, and it also showed that their applications are continuously increasing. Another significant result of the literature survey was that it would be more appropriate to use supercapacitors in parallel with the other storage devices. Thus, it seems appropriate to design a module that would get connected to 12 V, 24 V, and 48 V bus voltages in parallel for different utilizations of batteries and to study its performance. Also, it is possible to reserve peak loads and instantaneous currents using supercapacitors in many ways.

In conclusion, a module was designed by making use of 20 pieces of 310 F, 2.7 V supercapacitors. Chargedischarge tests for different load conditions were conducted for each capacitor and module. The changes observed in the current, voltage, and power were studied, and results were obtained about the amount of energy that could be stored and transferred to the load. Mathematical simulations and equivalent circuit models were also determined for this module, and the simulation results are repeated for different resistors in MATLAB/Simulink. The obtained experimental results showed that they conform to the simulation, catalog data, and expected theoretical results, and the modules designed could be used for several intended applications. The experimental results show that the supercapacitors have more superiority than conventional capacitors and other storage devices in many ways. A comparison timetable of experimental and simulation results for charge and discharge curve is given for the comments of all the results.

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Detailed measurement results for SC and module charge and discharge tests.

Time (second) 0 30 60 90 120 150 180 210 270 300 330 360 Charge Current (A) 2.20 2.00 1.90 1.80 1.60 1.30 1.31 1.13 1.13 1.08 1.04	Time (second) 0 30 60 90 120 180 210 200 30	0 30 60 90 120 180 210 270 300 330 360 2.20 2.00 1.90 1.80 1.40 1.30 1.13 1.13 1.04 1.04	0 30 60 90 120 180 210 240 270 300 330 360 20 2.00 1.90 1.80 1.40 1.30 1.13 1.13 1.04 1.04	CHARGE DISCHARGE TEST MEASUREMEN 30 60 90 120 180 210 240 270 300 330 360 .00 1.90 1.60 1.50 1.40 1.30 1.25 1.13 1.13 1.08 1.04	D 90 120 180 210 240 270 330 360 0 120 150 180 210 240 270 300 360 360 0 150 1.50 1.40 1.30 1.25 1.13 1.13 1.08 1.04	CHARGE - DISCHARGE TEST MEASUREMEN 120 150 210 240 270 300 360 10 1.50 1.50 1.30 1.25 1.30 300 360	CHARGE- DISCHARGE TEST MEASUREMEN 0 150 180 210 240 370 330 360 0 1.50 1.40 1.30 1.25 1.13 1.08 1.04	CHARGE-DISCHARGE TEST MEASUREMEN 1 180 210 240 300 330 360 1 140 1.30 1.25 1.13 1.08 1.04	GE- DISCHARGE TEST MEASUREMEN 210 240 270 300 330 360 1.30 1.25 1.18 1.13 1.04 1.04	SCHARGE TEST MEASUREMEN 240 270 300 330 360 1.25 1.18 1.13 1.08 1.04	IGE TEST MEASUREMEN 270 300 330 360 1.18 1.13 1.08 1.04	ST MEASUREMEN 300 330 360 1.13 1.08 1.04	ASUREMEN 330 360 L.08 1.04	07 09 00 MEN		S 80	420 0.98 (450 4	87 0	1 1 0	540 6	9 0.0	50 72	7 0.5	0 840 3 0.48	0.45 0.45	0.3	0 12	88
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Charge Power Calculation (W) 0 9.1 9.2 8.2 6.96 5.5	Charge Power Calculation (W) 0 9.1 9.2 8.2 6.96 5.5	w) 0 9.1 9.2 8.2 6.96 5.5 v	0 9.1 9.2 8.2 6.96 5.5	9.1 9.2 8.2 6.96 5.5	2 8.2 6.96 5.5	2 6.96 5.5	6 5.5	-	4.57	3.81	2.56										_	_	_						
Discharge Current (A) 20.9 8 4 1.8 0.8 0.4	Discharge Current (A) 20.9 8 4 1.8 0.8 0.4 0	20.9 8 4 1.8 0.8 0.4	0.9 8 4 1.8 0.8 0.4 0	8 4 1.8 0.8 0.4	4 1.8 0.8 0.4 0	8 0.8 0.4	8 0.4 (+	0.25	0.1	0.01										루	e mea	surum	ents o	in this	time	could		
Discharge Voltage (V) 2.85 0.9 0.5 0.27 0.15 0.08	Discharge Voltage (V) 2.85 0.9 0.5 0.27 0.15 0.08	2.85 0.9 0.5 0.27 0.15 0.08	85 0.9 0.5 0.27 0.15 0.08	0.9 0.5 0.27 0.15 0.08	5 0.27 0.15 0.08	27 0.15 0.08	5 0.08	8	0.05	0.03	0.01										ŭ	ot mad	e bica	use of	the o	vershi	oot of		
Discharge Power Calculation(W 59.57 7.2 2 0.49 0.12 0.03	Discharge Power Calculation(W 59.57 7.2 2 0.49 0.12 0.03	ו(w 59.57 7.2 2 0.49 0.12 0.03	57 7.2 2 0.49 0.12 0.03	7.2 2 0.49 0.12 0.03	2 0.49 0.12 0.03	9 0.12 0.03	2 0.03	~	0.01	0	0										su	percap	acitor	eddn s	erlimi	t valu	e		
Time (Second) 0 30 60 90 120 150	Time (Second) 0 30 60 90 120 150	0 30 60 90 120 150	0 30 60 90 120 150	30 60 90 120 150	0 90 120 150	0 120 150	0 150	0	180	210	240	270	300	330	360	390	420	450	8										
Charge Current (A) 11 8.5 5.5 4 3 2.3 1	Charge Current (A) 11 8.5 5.5 4 3 2.3 1	11 8.5 5.5 4 3 2.3 1	11 8.5 5.5 4 3 2.3 1	8.5 5.5 4 3 2.3 1	5 4 3 2.3 1	4 3 2.3 1	3 2.3 1	1	88	1.5	1.24	1	0.9	0.8 0	.65														
Charge Voltage (V) 0 5.15 8.9 10.1 11.2 12 1	Charge Voltage (V) 0 5.15 8.9 10.1 11.2 12 1	0 5.15 8.9 10.1 11.2 12 1	0 5.15 8.9 10.1 11.2 12 1	15 8.9 10.1 11.2 12 1	9 10.1 11.2 12 1	1 11.2 12 1	2 12 1	-	2.6	13.1	13.4	13.7	13.9	14 1	4.3														
Charge Power Calculation (W) 0 43.8 49 40.4 33.6 27.6	Charge Power Calculation (W) 0 43.8 49 40.4 33.6 27.6	w) 0 43.8 49 40.4 33.6 27.6	0 43.8 49 40.4 33.6 27.6	3.8 49 40.4 33.6 27.6	9 40.4 33.6 27.6	4 33.6 27.6	6 27.6	.0	23.7	19.7	16.7	13.7	12.5	11 9	.26														
Discharge Current (A) 11 7.5 6.8 4 3 1.9	Discharge Current (A) 11 7.5 6.8 4 3 1.9	11 7.5 6.8 4 3 1.9	11 7.5 6.8 4 3 1.9	7.5 6.8 4 3 1.9	8 4 3 1.9	4 3 1.9	3 1.9		1.2	0.8	0.55	0.36	0.25	0.2 0	.11	-	0.05	0	8										
Discharge Voltage (V) 14.25 8.5 8 4.6 3.2 2.15 1	Discharge Voltage (V) 14.25 8.5 8.6 3.2 2.15 1.	14.25 8.5 8 4.6 3.2 2.15 1.	25 8.5 8 4.6 3.2 2.15 1.	8.5 8 4.6 3.2 2.15 1	8 4.6 3.2 2.15 1.	6 3.2 2.15 1.	2 2.15 1.	17	45	0.9	0.6	0.4	0.28	0.2 0	.13		0.08	0	8										
Discharge Power Calculation(W 156.8 63.8 54 18.4 9.6 4.09 1.	Discharge Power Calculation(W 156.8 63.8 54 18.4 9.6 4.09 1.	ו(w 156.8 63.8 54 18.4 9.6 4.09 1.	5.8 63.8 54 18.4 9.6 4.09 1.	3.8 54 18.4 9.6 4.09 1.	4 18.4 9.6 4.09 1.	4 9.6 4.09 1.	6 4.09 1.	-i	74	0.72	0.33	0.14	0.07	0	.01		0		0										