

Hybrid Alopex based DECRPSO algorithm optimized Fuzzy-PID controller for AGC

Jyoti Ranjan Nayak*, Binod Shaw* and Binod Kumar Sahu**

*Department of Electrical Engineering, National Institute of Technology, Raipur, Chhattisgarh 492010, India

**Department of Electrical Engineering, ITER, Siksha 'O' Anusandhan University, Bhubaneswar 751030, India

*Corresponding author: bapi.jyoti.2@gmail.com

ABSTRACT

This paper corroborated the hybrid Alopex based Differential Evolution Craziness based Particle Swarm Optimization algorithm (ADECPSO) over DE, ADE, PSO, and CRPSO algorithms to pursuit the gain parameters of the PID and Fuzzy PID (FPID) controller. In a two-area thermal-hydro-diesel power system, primacy of FPID controller is endorsed with PID controller tuned with assorted optimization techniques. The hybrid ADECPSO algorithm is affirmed over the above mentioned algorithms to tune PID controller in a two-area hydro-thermal system. PSO, DE, CRPSO, ADE, and ADECPSO are executed individually to optimize the controller to enhance the transient analysis by conceding undershoot, overshoot, and settling time of the system. The compilation of advantages of alopex based DE and craziness based PSO causes an adequate hybrid algorithm, which enhances the performance of Automatic Generation Control (AGC). The step load uprise in area-1 is imposed to observe the activities of AGC. Undeniably, FPID controller optimized by ADECPSO commits superior performance over PSO, DE, CRPSO, and ADE optimized controller as proposed AGC system. The FPID controller optimized by ADECPSO, ADE, and CRPSO is realized in real time environment (OPAL RT OP5600). So, the modified mutation of DE by alopex scheme enhances the potentiality to tune the system variables.

Keywords: Automatic Generation control (AGC); Craziness based PSO (CRPSO); Differential Evolution (DE); Fuzzy PID (FPID); Hybrid Alopex based Differential Evolution craziness based Particle Swarm Optimization (ADECPSO) algorithm.

INTRODUCTION

Interconnection of the system is an imperative arrangement to attain the load demand growing with a brisk proportion. Interconnection enhances the stability, cost-effectiveness and also utilizes the generating stations sublimely. The prime function of the interconnected power system is to equipoise the power generated with the load demand associated with the loss (Kundur et al., 1994). Small load variation consequences the deviations of system frequency and power from alleged value and transmitted to other areas, which may cause abominable effects. To yield the power economically, stably, and reliably in interconnected power system, it is requisite to fix the system frequency and tie-line power deviations to their scheduled values (Kundur et al., 1994; Cohn, 1956; Fosha, 1970). AGC is a vital character to resolve the above problem. AGC acts as a secondary controller in the power system. This control mechanism is applicable to regulate the basic functions to:

- i. Enhance the trait of transmitted power economically and reliably.
- ii. Enhance the ability to impasse the deviations of frequency and tie-line power to zero (i.e. $\Delta f = \Delta P_{tie} = 0$).
- iii. Minimize the function concerning overshoot (O_{sh}), undershoot (U_{sh}) and settling time (T_s).

Many researchers have introduced lots of various controllers and optimization techniques to amend the performance of the AGC. Kumar et al. (2005) have highlighted the various control strategy adopted to enhance the performance of AGC for last few decades. Khodabakhshian et al. (2010) and Shabani et al. (2013) have proposed the PID controller as AGC of hydro power plant and a robust PID controller in a two-area interconnected power system optimized by ICA respectively. Intelligent cascade consolidation of PI-PD and 2-DOF PID enhances the performance of AGC over conventional PID controllers analyzed (Dash et al., 2016; 2014; Sahu et al., 2016). For last few decades many researchers have concluded the Fuzzy Logic Controller (FLC) as a predominant controller than other traditional controllers proposed by Zadeh (1965). The cascade aggregation of FLC and PID (FPID) optimized by various optimization techniques enhances the performance of the system, which is well described in Chown et al. (1997); Yesil et al. (2004); Nayak et al. (2015a; 2016; 2018b); Sahu et al. (2016); Sahu B.K. et al. (2014; 2015; 2016). In Nayak et al. (2018a), cascade PD-FOPID optimized by GHS is validated. Many novel and hybrid optimization techniques have also been proposed like ABC, GWO, BA, PSO-PS, FA-PS, GS-PS, BF-PSO, and ASOS in (Gozde et al. (2012); Guha et al. (2016); Dash et al. (2015); Sahu et al. (2015a; 2015b; 2015c); Nanda et al. (2009); Nayak et al. (2018c). Kennedy et al. (1995) have introduced a swarm based technique entitled as PSO (Particle Swarm Optimization) and Ghosal (2004) has adopted this technique to improve the performance of AGC by optimizing the gain parameters of PID controllers. Panda et al. (2013) have composed BFOA (Bacteria Foraging Optimization Algorithm) and PSO to enhance the nonlinear power system. Storn et al. (1997) have introduced an evolutionary algorithm DE and Rout et al. (2013) have modeled AGC to analyze DE. Sahu et al. (2014) and Nayak et al. (2015b) have investigated the performance of FPID and T2FPID controller in AGC optimized by hybrid DEPSO algorithm proposed by Zhang et al. (2003). Hybrid DECRPSO algorithm is implemented to tune FPID controller in LFC Nayak et al. (2017).

In the present work, PID controller is adopted to validate the performance of the FPID controller of the system as AGC. The performance of the system is enormously influenced by the parameters of the controller. For the purpose to attain these parameters to enhance the system parameters, adoption of optimization technique is very imperative ingredient. PSO, craziness based PSO, DE, alopex based DE, and hybrid ABDECRPSO algorithms are adopted to tune the controller variables. The comparative analysis is concluded by implementing the proposed approach in three different power system models such as thermal-hydro-diesel, thermal-hydro, and thermal-hybrid power systems. The hybrid ABDECRPSO algorithm is concluded as better algorithm among the above-mentioned algorithms. The basic aspects of design of the proposed work are as follows:

1. To design power system model with thermal plant in area-1 and hydro-diesel plant in area-2.
2. To design the controllers to be imposed in each area.
3. To design optimum controller by adopting convenient optimization techniques.

SYSTEM INVESTIGATED

The explored system is a two-area non-reheat thermal-hydro-diesel power system. Area1 is owing equivalent transfer function blocks of non-reheat thermal power station and area-2 is owning hydro and diesel power stations equivalent model as portrayed in Fig. 1. The power system parameters are expressed in appendix-1. Area Control Errors (ACEs) concerning deviations in frequency and tie-line power are formulated as interpreted in equation (1).

$$ACE_i = B_i \Delta f_1 + \Delta P_{tie,ij} \quad (1)$$

where 'i' and 'j' are the corresponding area and different area, respectively. B is the bias constant. A small step disturbance of 10% (0.1) is implemented in area 1 (ΔP_{D1}) to observe the performance of the controllers.

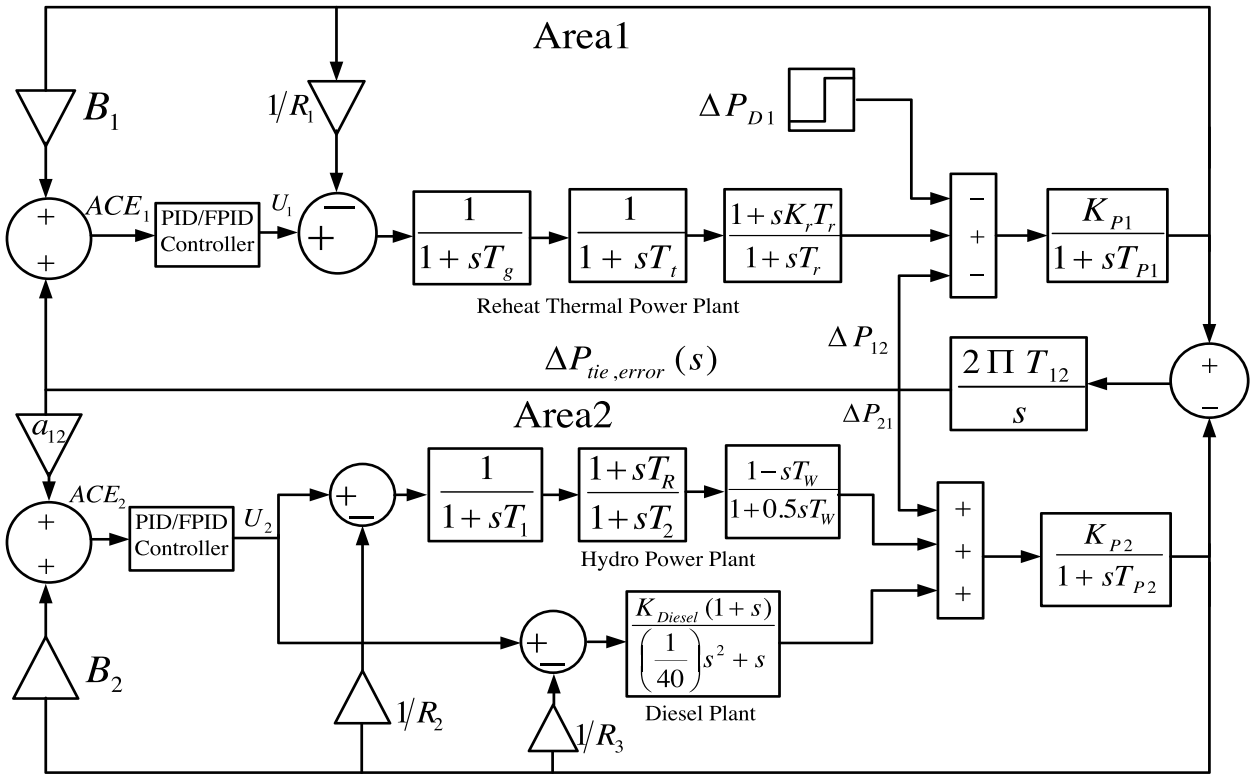


Figure 1. Interconnected hydro-thermal-diesel power system model.

The prime target of controller in this system is to set ACE to zero. For this purpose PID and fuzzy PID (FPID) controllers are imposed in both areas. The inputs to the controller in one area are the ACEs of that respective area and the outputs are U_1 , U_2 , and U_3 . The objective function adopted for this proposed model is ITAE (Integral Time Absolute Error) by concerning Δf_1 , Δf_2 , and ΔP_{tie} . ITAE is adopted to reduce overshoot, undershoot, and settling time of the system. In ITAE, the severity of the errors gradually increases with respect to time. So ITAE is a better cost function to concern the transient performance of the system. PID and FPID controllers are adopted to lessen the ITAE value of the system.

ITAE is mathematically formulated as portrayed in equation (2).

$$ITAE = \int_0^{t_{sim}} (|\Delta f_1| + |\Delta f_2| + |\Delta P_{tie}|) \cdot t \cdot dt \tag{2}$$

To achieve the better ITAE value, it is significant to choose the gain parameters of the controller by adopting convenient optimization techniques.

CONTROLLER STRUCTURE

The design of controller is also significant to enhance the performance of the system. PID and FPID controllers are employed individually in both the areas. Many researchers have validated the superiority of FPID controller than traditional PID controller. The framework of PID and FPID controllers is portrayed in figure 2 and figure 3, respectively.

Table 1. Rule structure.

ACE	ΔACE				
	HN	LN	M	LP	HP
HN	HN	HN	LN	LN	M
LN	HN	LN	LN	M	LP
M	LN	LN	M	LP	LP
LP	LN	M	LP	LP	HP
HP	M	LP	LP	HP	HP

The Mamdani max-min inference system is adopted as inference engine and center of Gravity (COG) approach is adopted as defuzzification of processed data. The rule structure is characterized in table1. The operation of the FLC is illustrated in figure 5. Fuzzy Logic Controller (FLC) is superior over PID to control non-linear, imprecise and uncertain information. Two trapezoidal membership functions (MFs) and three triangular MFs entitled as Highly Negative (HN), Less Negative (LN), Middle (M), Less Positive (LP), and Highly Positive (HP) are used as illustrated in figure 4.

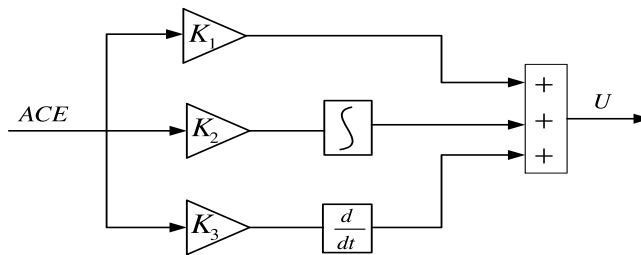


Figure 2. PID controller structure of area 1.

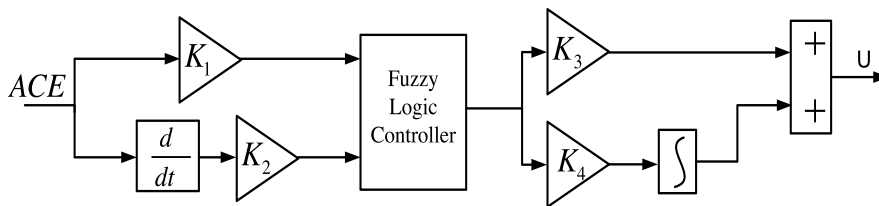


Figure 3. Fuzzy PID controller structure of area 1.

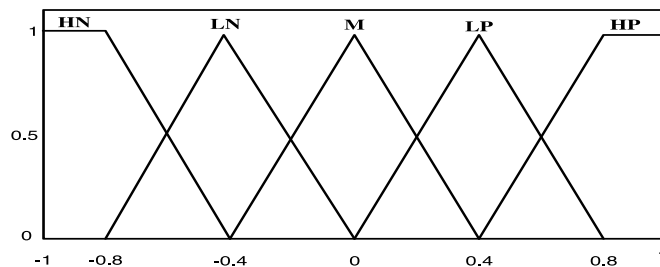


Figure 4. Membership functions of FLC.

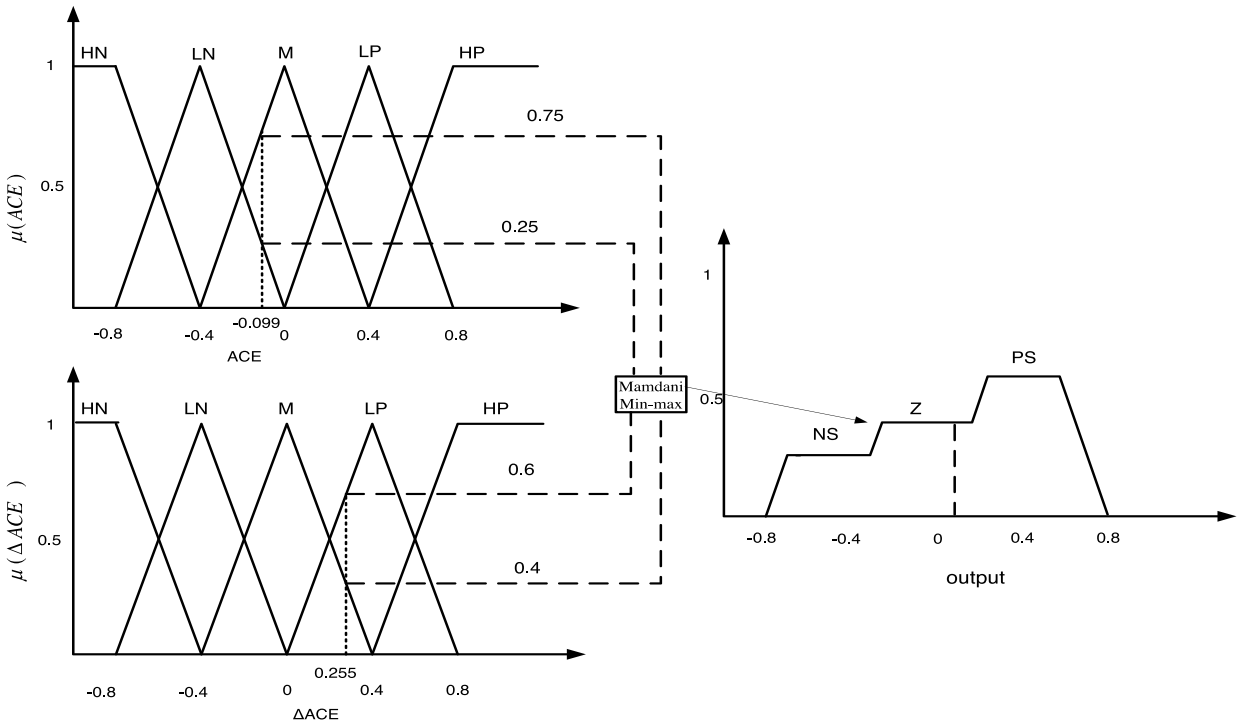


Figure 5. Mamdani min-max operation of FLC.

HYBRID ALOPEX-BASED Differential Evolution Craziness based Particle Swarm Optimization (ADECRPSO)

A novel hybrid ADECRPSO algorithm is validated with various optimization techniques (DE, ADE, PSO, and CRPSO) to tune the design variables of FPID controller to enhance the performance of proposed system. Differential Evolution (DE) is an evolutionary algorithm illustrated in Storn et al. (1997). DE is established by concerning three significant stages like mutation, crossover, and selection. The population in DE is accelerated with very immense diversity factor. There may be a probability to ambush into local optima due to huge diversity and inadequacy memory of DE. To enhance the performance, mutation of DE algorithm is modified by alopex based strategy as characterized in Tzanakou et al. (1979). This altered mutation strategy assists to discover the probability of direction by correlating fitness of two distinct individuals. This strategy enhances the range of the search space and is defined in Leon (2017).

PSO is a swarm based algorithm proposed by Kennedy et al. (1995). PSO is mostly established by concerning the particle’s own best (P_{Best}) and the best among all particles (G_{Best}). The memory of this algorithm to store last best value and the current best value makes this algorithm precise. The bizarre movement of the fish and bird colony is narrated to customize the velocity expression of PSO and is established as craziness based PSO (CRPSO) (Kar et al., 2012; Saha et al., 2013; Upadhyay et al., 2014). The balance between exploration and exploitation is maintained by using the random values and their mirror values to alter the velocity. The preeminent goal of this work is to establish a hybrid algorithm by concerning the advantages of both ADE and CRPSO algorithms. The worst particles in each iteration are replaced by randomly generated particles to yield higher probability to get optimal solution. The parameters of the algorithm are illustrated in appendix-2 and the flow chart of ADECRPSO is portrayed in figure 6.

The steps pursued by this hybrid ADECRPSO algorithm are as follows:

1. Initialize the population i.e. $[X]_{NP \times D}$.
2. Initialize the velocity of the particles of the population for PSO i.e. $[V]_{NP \times D}$.
3. Set F , CR , $V_{craziness}$, C_1 , C_2 .
4. Set $T=1$.
5. Alopex based DE operation
 - i. Mutation

Correlation (C) between two random individuals $A = (a_1, a_2, \dots, a_D)$ and $B = (b_1, b_2, \dots, b_D)$ is calculated as characterized in equation (3).

$$C_{i,j} = (a_j - b_j)[f(A) - f(B)] \tag{3}$$

where $i = 1, 2, \dots, NP$ and $j = 1, 2, \dots, D$. $f(A)$ and $f(B)$ are the functional values of individuals A and B, respectively.

Temperature (T) is the mean value of correlation vectors of last generation and is characterized in equation (4).

$$T = \frac{1}{D} \frac{1}{NP} \sum_{i=1}^{NP} \sum_{j=1}^D |C_{i,j}| \tag{4}$$

The probability of negative direction may be characterized as in equation (5).

$$P_j = \frac{1}{1 + e^{\frac{c_j}{T}}} \tag{5}$$

The movement direction is described mathematically in equation (6).

$$\delta_j = \begin{cases} 1 & \text{If } P_j \geq rand \\ -1 & \text{Otherwise} \end{cases} \tag{6}$$

The mutation is estimated by using equation (7).

$$V_{i,j} = a_j + \delta_j \cdot |a_j - b_j| \cdot F \tag{7}$$

- ii. Crossover

Offspring vector (V) is characterized by concerning crossover rate (CR) in equation (8).

$$U_{i,j} = \begin{cases} V_{i,j} & \text{If } rand \leq CR \\ X_{i,j} & \text{Otherwise} \end{cases} \tag{8}$$

- iii. Selection

The particles with better fitness value are selected as target vector as characterized in equation (9).

$$X_{i,j} = \begin{cases} U_{i,j} & \text{If } f(U_{i,j}) \leq f(X_{i,j}) \\ X_{i,j} & \text{If } f(X_{i,j}) \leq f(U_{i,j}) \end{cases} \tag{9}$$

6. Craziness based PSO

- i. Identify the individual best (P_{best}) and best among individual best (G_{best}).
- ii. Velocity of the particle is defined in equation (10).

$$V_i^{k+1} = r_2 \times S_{r_3} \times V_i^k + (1 - r_2) \times c_1 \times r_1 (P_{best} - X_i) + (1 - r_2) \times c_2 \times (1 - r_1)(G_{best} - X_i) \quad (10)$$

$$\text{Where, } S_{r_3} = \begin{cases} -1 & \text{If } r_3 \geq 0.05 \\ 1 & \text{Otherwise} \end{cases}$$

Velocity is modified by conceding craziness factor as in equation (11).

$$V_i^{k+1} = V_i^{k+1} + P_{r_4} \times S_{r_4} \times V_{craziness} \quad (11)$$

$$\text{Where } P_{r_4} = \begin{cases} 1 & \text{If } r_4 \geq P_r \\ 0 & \text{Otherwise} \end{cases}$$

$$\text{and } S_{r_4} = \begin{cases} -1 & \text{If } r_4 \geq 0.5 \\ 0 & \text{Otherwise} \end{cases}$$

r_1, r_2, r_3 and r_4 are the random numbers [0 1].

The particle position is altered as in equation (12).

$$X_{i,new} = X_i + V_i \quad (12)$$

The particle position is updated by concerning fitness values as in equation (13).

$$X_{i,j} = \begin{cases} X_{i,new} & \text{If } f(X_{i,new}) \leq f(X_i) \\ X_i & \text{Otherwise} \end{cases} \quad (13)$$

7. The worst particles are replaced by the random particles to enhance the probability to extract optimum point. The numbers of worst particles are decided by using equation (14) and replaced by new particles as described in equation (15).

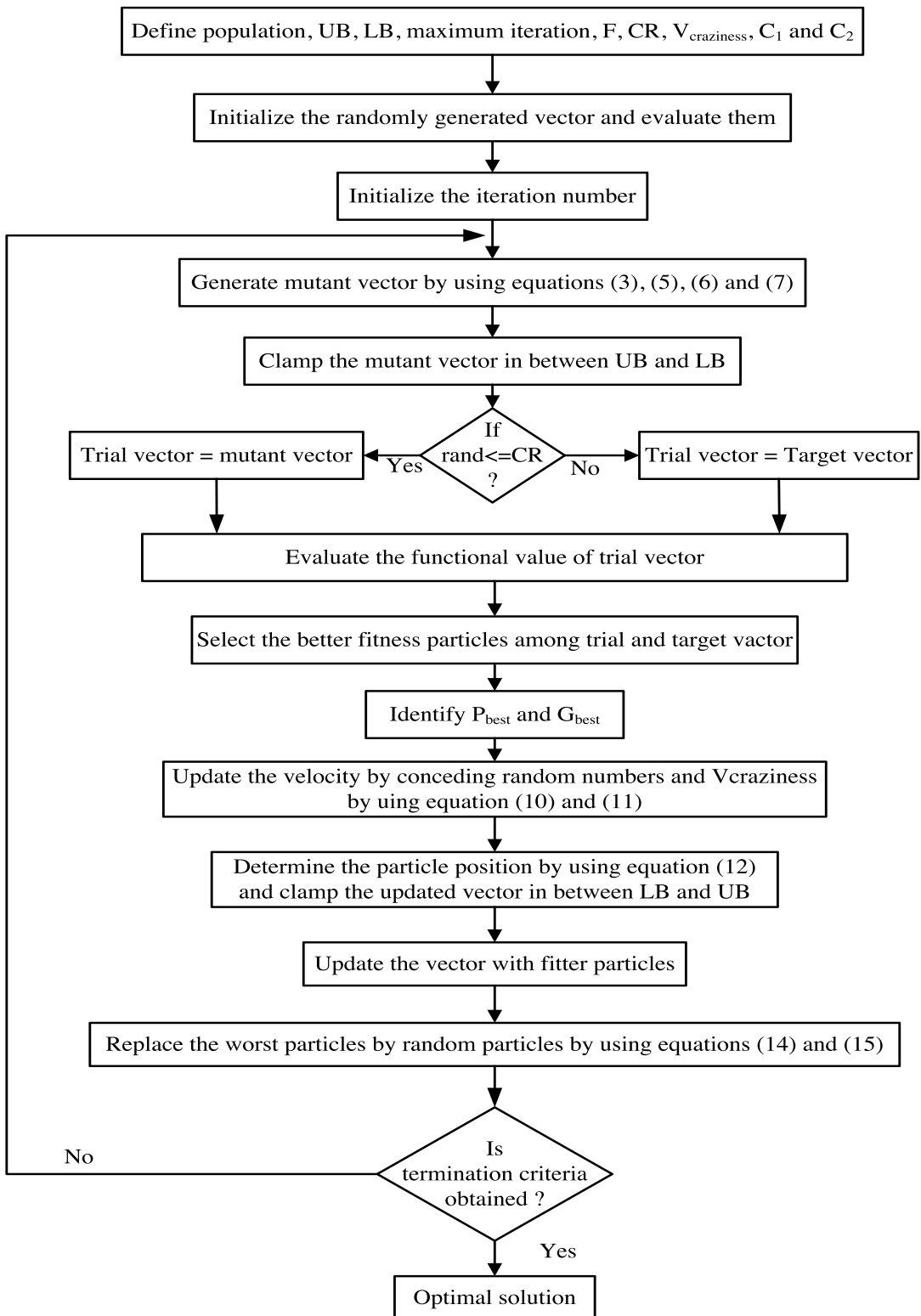


Figure 6. Flow chart of hybrid ADECRPSO algorithm.

$$N = find((f(G_{Best}) + M) < f(X_i)) \tag{14}$$

$$X_i(N) = \min(X_i) + rand \times (\max(X_i) - \min(X_i)) \tag{15}$$

where N and M are the number of particles to be replaced and the threshold value beyond which particles are to be replaced, respectively.

8. The iteration is updated by one and repeats the steps 5 and 7 until maximum iteration.

RESULT AND DISCUSSION

Transient performance analysis

This paper is proposed to validate the proficiency of the novel hybrid Alopex based Differential Evolution Craziness based Particle Swarm Optimization (ADECPSO) to tune the scaling factors of PID and FPID controller. PSO, DE, CRPSO, and ADE are adopted to investigate the performance of hybrid ADECPSO algorithm. All the algorithms are executed individually to optimize the parameters of controller with number of population 50 and maximum iteration as 100. PID controller is optimized by only ADECPSO algorithm to portray the proficiency of FPID controller. The fundamental goal of AGC is to lessen the objective function (ITAE) or to set the ACE to zero.

To interpret the activity of the AGC a load disturbance of 10% (0.1) is applied in area 1. The gain parameters of conventional PID controller optimized by ADECPSO algorithm are as $K_1 = 1.9175$, $K_2 = 1.5822$, $K_3 = 0.9092$ in area 1 and $K_1 = 0.6735$, $K_2 = 0.1276$, $K_3 = 1.4844$ in area-2, respectively. The gain factors of FPID controller tuned by assorted algorithms are illustrated in table 2. The proposed objective function is a multi-variable with boundary constraint as

$$0.01 \leq K_i \leq 2 \quad i = 1, 2, \dots, D$$

where D is the number of gain parameters of the controllers.

Table 2. Optimal gain parameters of FPID controller optimized by different Optimization techniques.

Optimization Techniques	Gain parameters of FPID controllers							
	Area-1				Area-2			
	K ₁	K ₂	K ₃	K ₄	K ₁	K ₂	K ₃	K ₄
ADECPSO	2.0000	1.1063	1.9892	2.0000	1.3646	1.4525	1.9999	2.0000
ADE	2.0000	1.2016	1.5036	1.9998	2.0000	0.7802	1.3877	1.1114
CRPSO	2.0000	2.0000	0.7568	2.0000	0.0100	1.5243	0.0100	1.6908
DE	2.0000	0.8489	1.5728	2.0000	1.6070	1.1775	0.7770	1.4380
PSO	2.0000	0.8831	1.3569	2.0000	0.7676	1.0293	1.6599	0.3983

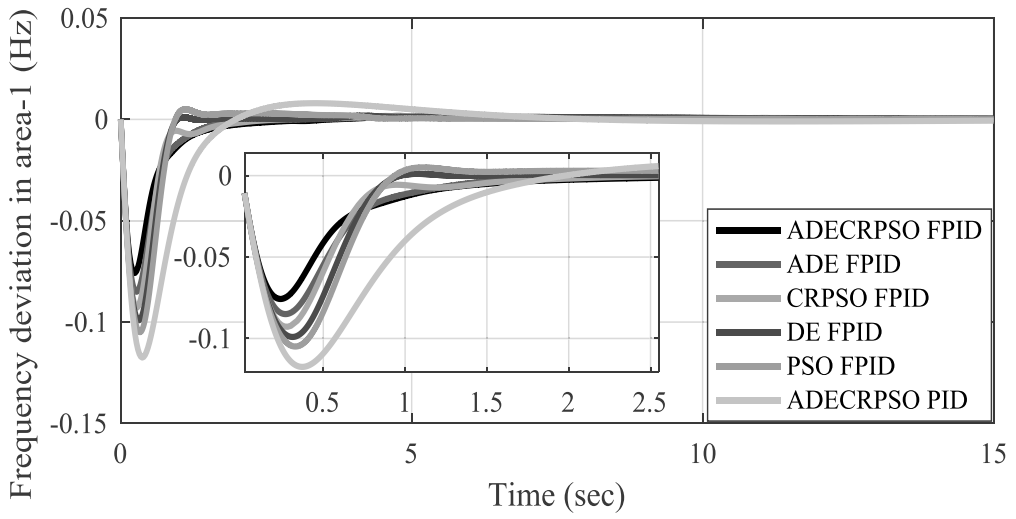


Figure 7. Frequency deviation in area 1 (Hz).

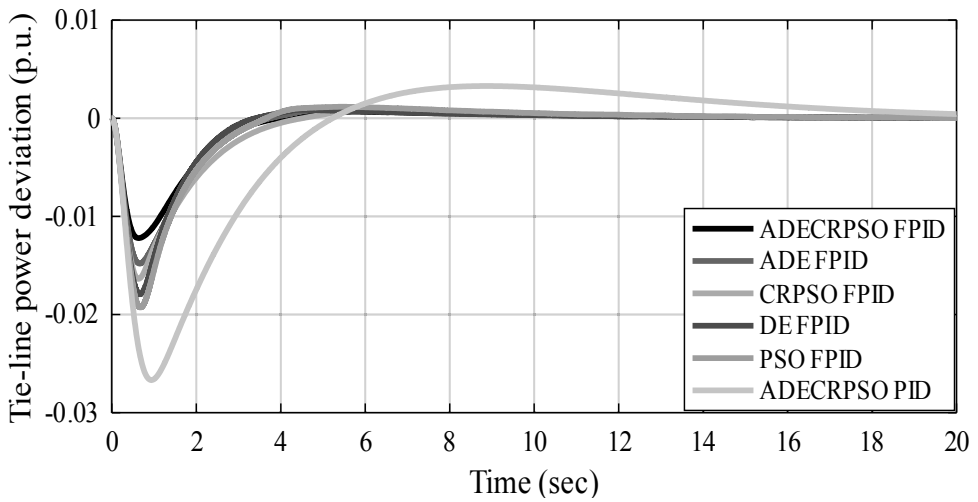


Figure 8. Frequency deviation in area2 (Hz).

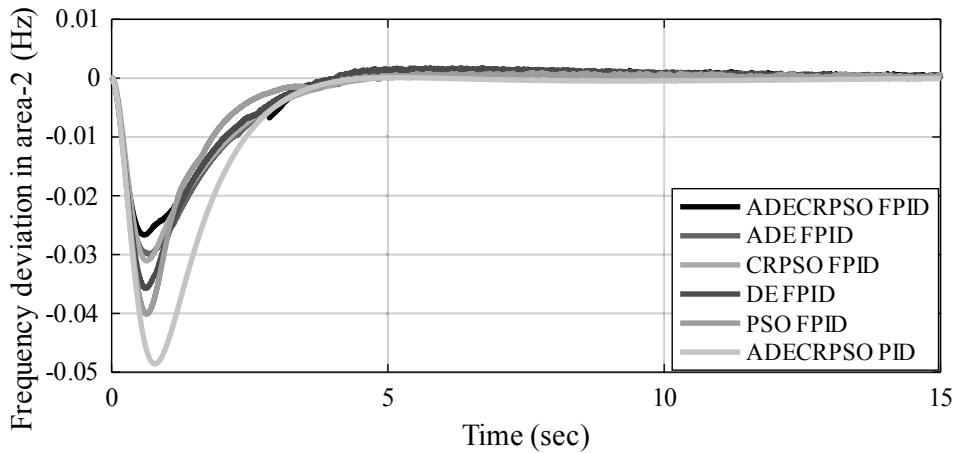


Figure 9. Tie-line power deviation in p.u.

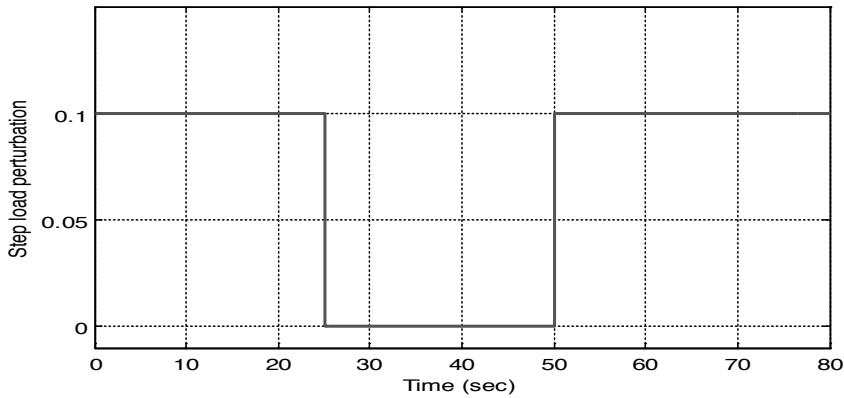


Figure 10. Variable SLP.

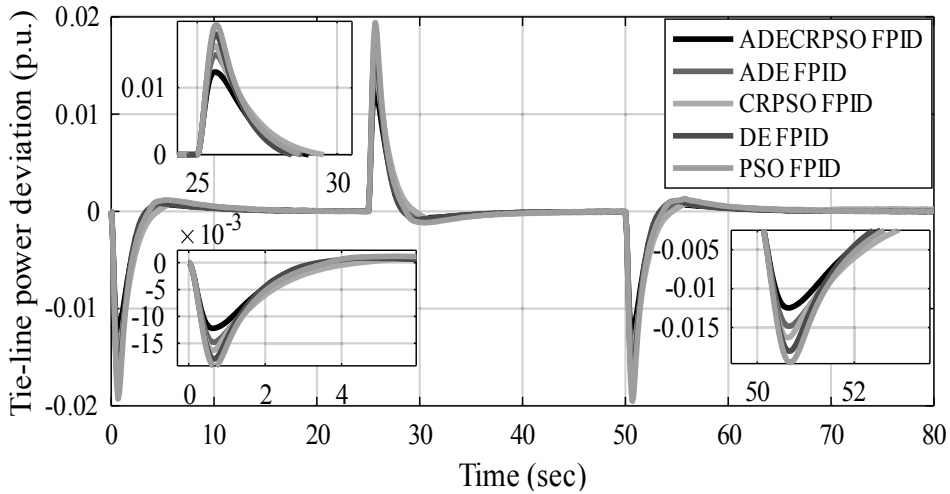


Figure 11. Tie-line power deviation in p.u. with variable SLP.

The deviations of frequency of both area 1 & area 2 (Δf_1 and Δf_2) and tie-line power deviation (ΔP_{tie}) are illustrated in figure 7, figure 8, and figure 9. These figures provide a clear portrait that the response of hybrid ADECRPSO optimized FPID controller is better among all optimization techniques used in this paper. Table 3 encloses the substantial values of undershoot (U_{sh}), overshoot(O_{sh}), and settling time (T_s) of the responses.

Table 3. Response parameters of Δf_1 , Δf_2 , and ΔP_{tie} in the power system controlled by PID and FPID controller.

Optimization Techniques	Undershoot($U_{sh} \times 10^{-3}$) in p.u.			Overshoot($O_{sh} \times 10^{-3}$) in p.u.			Settling Time (T_s) in sec		
	Δf_1	Δf_2	ΔP_{tie}	Δf_1	Δf_2	ΔP_{tie}	Δf_1	Δf_2	ΔP_{tie}
ADECRPSO FPID	-75.7543	-26.6676	-12.2101	1.6788	1.5736	0.6746	6.4429	12.3945	7.7508
ADE FPID	-85.0208	-30.0053	-14.8024	1.6813	1.5916	0.8519	4.2794	15.0504	7.7925
CRPSO FPID	-92.7974	-31.1076	-16.3718	1.7852	1.6041	0.8558	8.4861	15.7416	8.2815
DE FPID	-99.0610	-35.6975	-17.9245	1.8633	1.7619	0.8688	8.5438	17.5158	9.9979
PSO FPID	-104.9229	-40.0832	-19.2711	5.0456	1.9114	1.1812	8.8058	27.7851	10.2678
ADECRPSO PID	-117.4496	-48.5940	-26.6729	7.9769	0.1579	3.2888	13.335	15.9945	19.4725

The values U_{sh} , O_{sh} , and T_s of hybrid ADECRPSO optimized PID controller are tabulated in table 3. The validation of proposed algorithm based FPID controller is realized in real time environment. The setup of OPALRT OP5600 is illustrated in figure 12. The responses of ADECRPSO, ADE, and CRPSO based FPID controller are portrayed in figures 13-15. The response of tie-line power deviation with a variable step load disturbance is as portrayed in figure 11 and the step load is portrayed in figure 10. The variable SLP is illustrated in figure 9. The ITAE value of hybrid ADECRPSO optimized PID controller is 0.8530 and the functional value of FPID controller optimized by various algorithms is tabulated in table 4. All the tables and figures yield a clear portrayal that hybrid ADECRPSO optimized FPID controller gives better transient response in two-area interconnected power system.



Figure 12. OPAL RT (OP5600) setup.

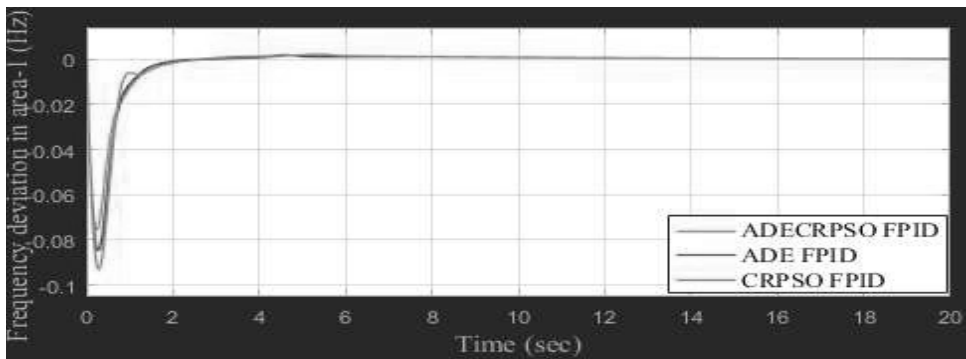


Figure 13. frequency deviation in area-1 in OPAL RT.

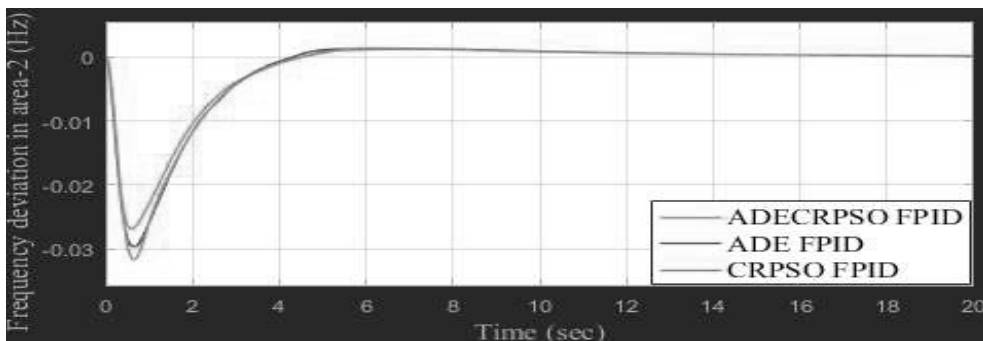


Figure 14. frequency deviation in area-2 in OPAL RT.

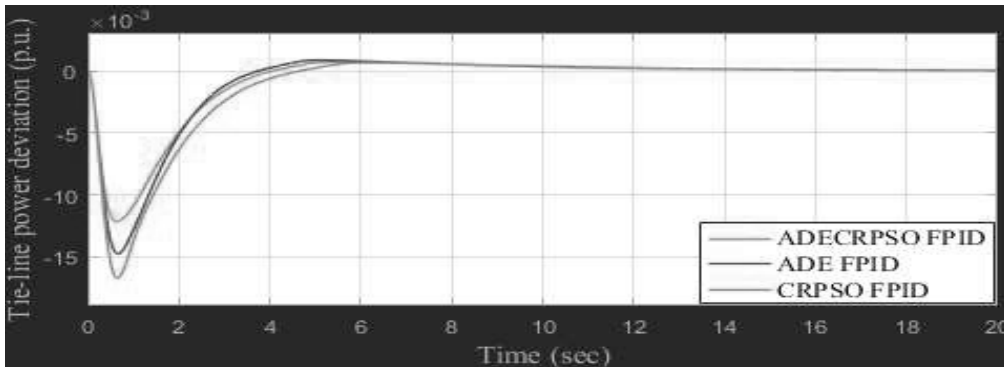


Figure 15. Tie-line power deviation in OPAL RT.

Table 4. Objective functions (ITAE) value for FPID controller optimized by various optimization techniques.

Optimization Techniques	Functional Values (ITAE)
ADECRPSO	0.3162
ADE	0.3190
CRPSO	0.3549
DE	0.3613
PSO	0.3666

Validation of proposed algorithm

To cater an equitable contrast between different algorithms tuned PID controller, two-area hydro-thermal power system tuned by hGGSA-PS (Khadanga et al., 2017) and hFA-PS (Sahu et al., 2015b) is adopted. Both areas consists of two equal characteristics hydro and reheat thermal units as portrayed in figure 16 and the system parameters are illustrated in appendix-3. The proposed algorithm is validated by enforcing a small disturbance of 0.015 p.u and the responses of frequency and tie-line power deviations are portrayed in figure 17, figure 18, and figure 19. The controller variables are tabulated in table 5. The numerical values of response parameters are tabulated in table. 6. In this section, superiority of alopex based mutation is validated to tune PID controller. Table 7 and figure 17, figure 18, and figure 19 endow an unequivocal interpret about the novelty of alopex based mutation of DE and its hybridization with CRPSO algorithm over DE, PSO, and CRPSO algorithms to yield better performance of the system.

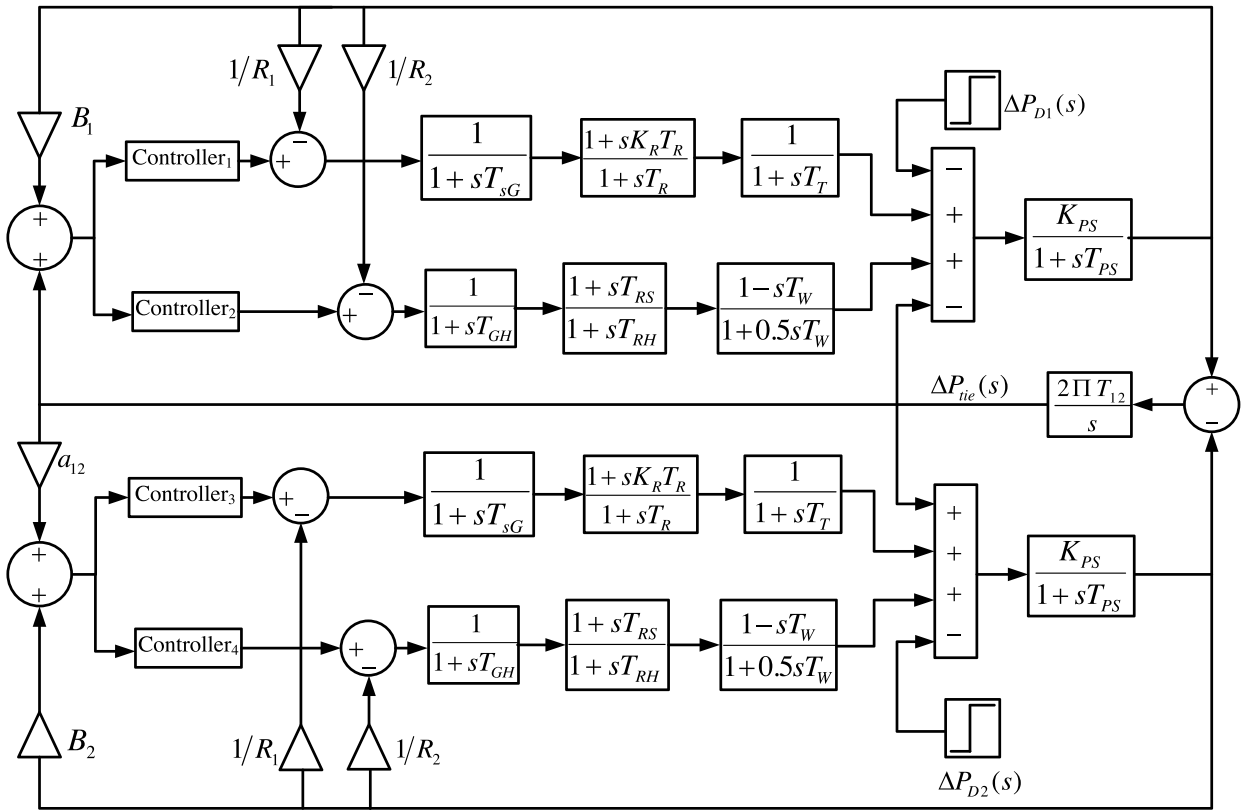


Figure 16. Transfer function model of the two-equal-area hydro-thermal interconnected power system (Khadanga et al., 2017; Sahu et al., 2015b).

Table 5. Optimal parameters of PID and FPID controller tuned by different Optimization techniques.

Optimization Techniques	Gain parameters of FPID and PID controllers															
	Area-1								Area-2							
	Thermal				Hydro				Thermal				Hydro			
	K ₁	K ₂	K ₃	K ₄	K ₁	K ₂	K ₃	K ₄	K ₁	K ₂	K ₃	K ₄	K ₁	K ₂	K ₃	K ₄
ADECRPSO FPID	2.0000	1.4179	1.9791	1.9989	2.0000	0.0972	1.7644	1.6064	1.7140	1.7325	1.7318	1.2623	1.5548	1.9994	0.3702	1.9315
ADECRPSO PID	2.0000	2.0000	1.1135		0.7636	0.0100	0.9700		1.3254	1.1753	0.3309		0.0100	1.0000	1.6236	
ADE PID	1.9189	2.0000	1.0128		1.0063	0.4793	1.8677		1.1871	2.0000	0.4706		0.2221	1.4819	0.2393	
CRPSO PID	1.3113	1.9256	0.7442		0.8581	0.7609	0.4874		2.0000	0.7900	1.2636		0.8147	0.6056	0.4363	
DE PID	1.2550	1.2348	0.6462		0.3846	0.4710	0.8567		1.0944	0.3198	0.9124		0.8245	0.8263	0.6663	
PSO PID	1.2705	1.0037	0.5926		0.3983	0.6319	0.4071		0.8953	0.2833	0.1577		0.7387	0.9399	1.4412	

Table 6. Response of Δf_1 , Δf_2 , and ΔP_{tie} in the power system controlled by PID and FPID controller optimized by various algorithms.

Optimization Techniques	Undershoot ($U_{sh} \times 10^{-3}$) in p.u.			Overshoot ($O_{sh} \times 10^{-3}$) in p.u.			Settling Time (T_s) in sec		
	Δf_1	Δf_2	ΔP_{tie}	Δf_1	Δf_2	ΔP_{tie}	Δf_1	Δf_2	ΔP_{tie}
ADECRPSO FPID	-3.2492	-1.0165	-0.3943	0	0	0	1.32	2.21	2.14
ADECRPSO PID	-10.3912	-4.5375	-1.6993	0	0	0	2.65	4.24	3.54
ADE PID	-11.6964	-5.1129	-1.8312	0	0	0	2.66	4.24	3.54
CRPSO PID	-12.7112	-5.6366	-2.2490	0.4299	0	0.0426	3.71	4.96	4.45
DE PID	-14.9495	-6.7548	-2.7182	0	0	0	4.03	5.31	4.25
PSO PID	-14.9545	-7.6455	-2.9389	0	0	0	4.97	6.13	5.10
hGGSA-PS PID (Khadanga et al., 2017)	-12.7126	-5.6532	-2.1601	0	0	0	3.15	4.52	4.02
hFA-PS PID (Sahu et al., 2015b)	-13.8942	-6.6224	-2.3886	0	0	0	3.42	4.98	4.15

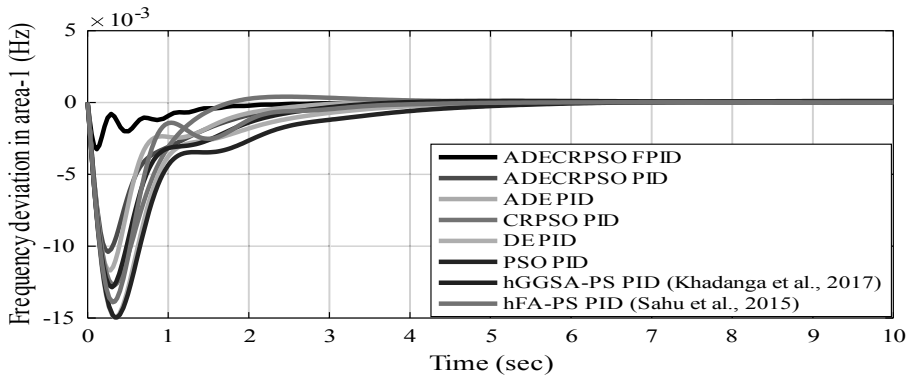


Figure 17. Frequency deviation in area1 (Hz) of two-area hydro-thermal power systems.

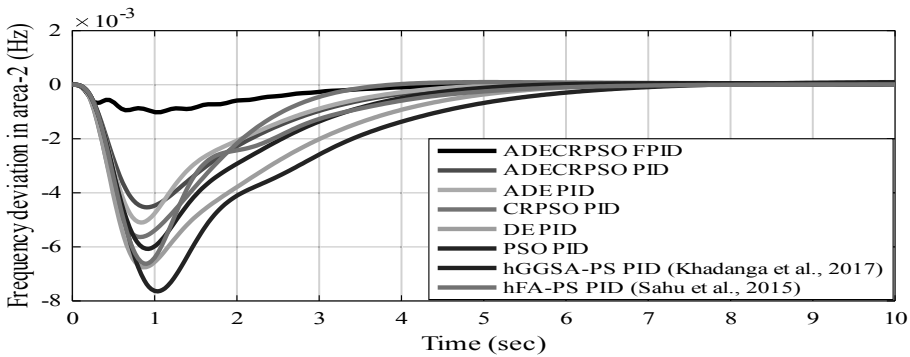


Figure 18. Frequency deviation in area2 (Hz) of two-area hydro-thermal power system.

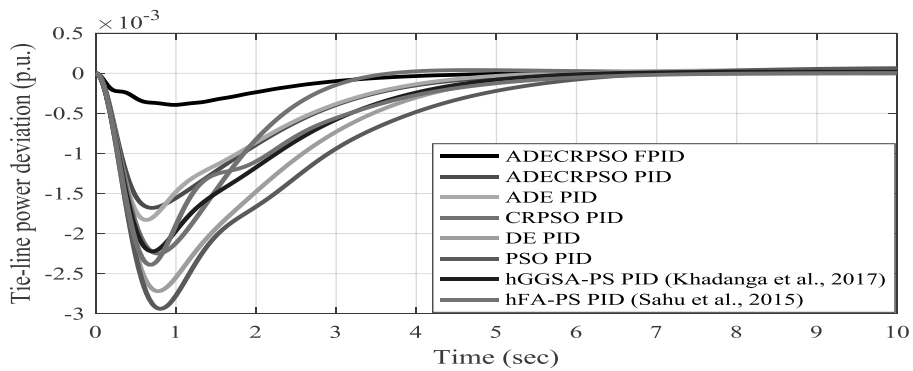


Figure 19. Tie-line power deviation (p.u.) of two-area hydro-thermal power system.

Further, the proposed ADECRPSO optimized FPID controller is substantiated by comparing with ASOS (Nayak et al. 2018c) and BFOA (Arya et al., 2017) optimized FPID controller. The deviations of the system with 1.5% step load in area-1 are portrayed in figures 20-22.

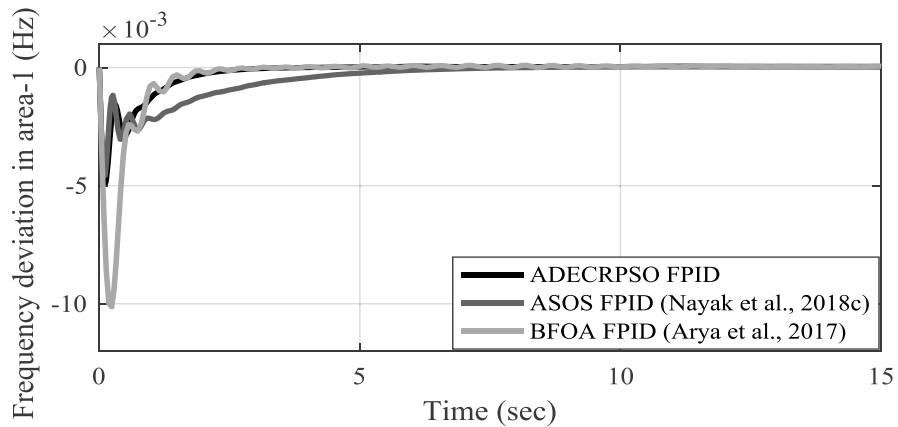


Figure 20. Frequency deviation in area-1 for 1.5% step load in area-1.

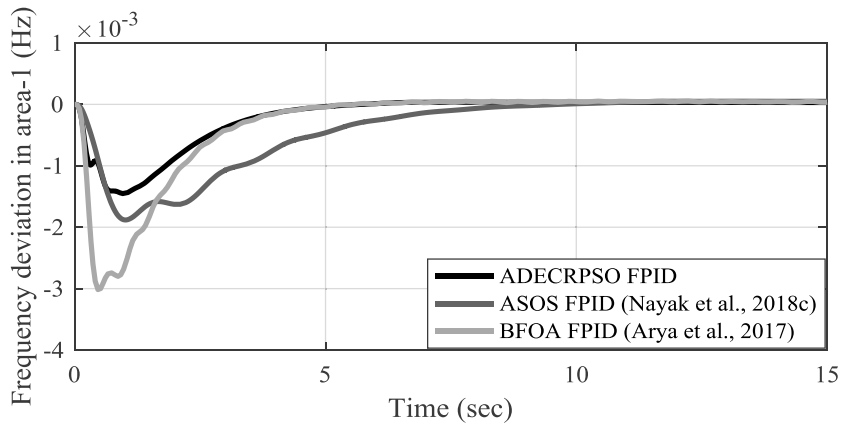


Figure 21. Frequency deviation in area-2 for 1.5% step load in area-1.

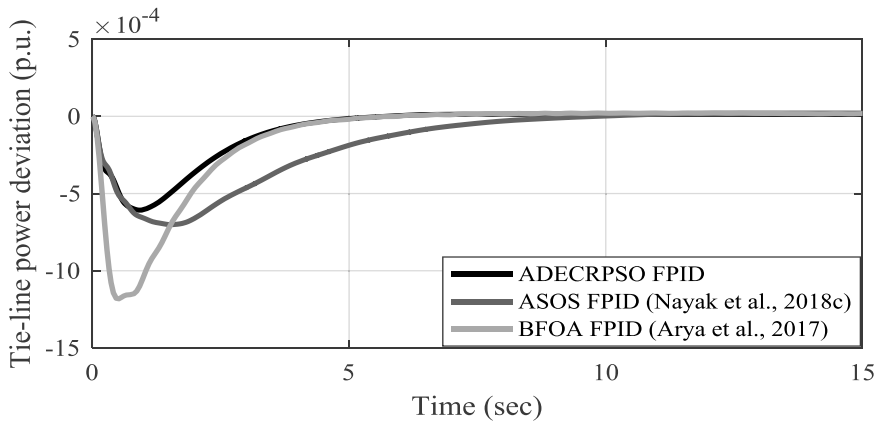


Figure 22. Tie-line power deviation for 1.5% step load in area-1.

Extension to other power system model

Further, the validation of acceptability of proposed algorithm is realized by implementing in a three-area thermal-hybrid power system. Thermal power generation unit by conceding physical constraint such as Governor Dead Band (GDB), Reheat turbine, and Boiler Dynamics (BD) is implemented in each area of the power system. Solar Power generation (SPG), Wind Power generation (WPG), Fuel Cell (FC), Aqua Electrolyzer (AE) (Sanki et al. 2018), Diesel Engine (DE), and Battery Energy Storage System (BESS) are implemented as distributed power generation (DPGs) in each area along with reheat thermal power generation unit as depicted in figure 23 (a). The transfer function models of BD and DPGs are illustrated as figure 23 (b) and (c), respectively. The generation capacities of area-1, area-2, and area-3 are in the ratio of 1:3:5, respectively. The power system parameters are indicated in appendix-4. The analysis is realized by implementing 1% in area of the power system. DE, PSO, CRPSO, ADE, and ADECRPSO are executed individually to tune PID controller parameters to minimize ITAE and the optimal gains of PID controllers are tabulated in table 7. The ADECRPSO tuned parameters of FPID controllers are tabulated in table 7. The system responses are realized by comparing the PID and FPID controllers optimized by different optimization techniques. The system responses of deviations of frequency and tie-line power are portrayed in figure 24-26.

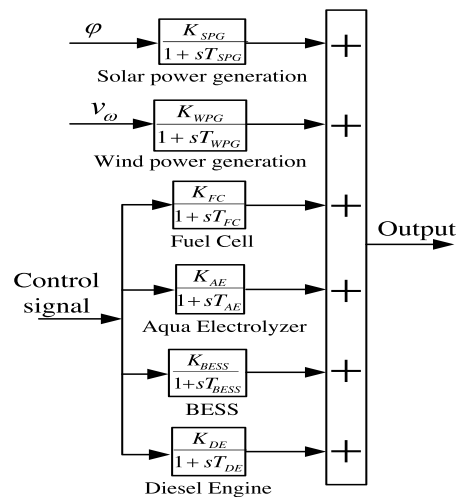
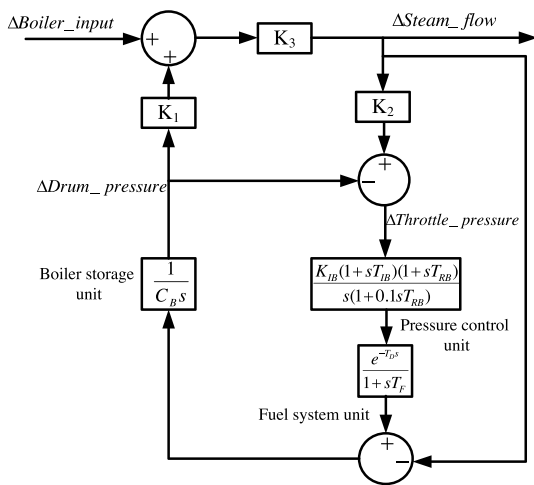
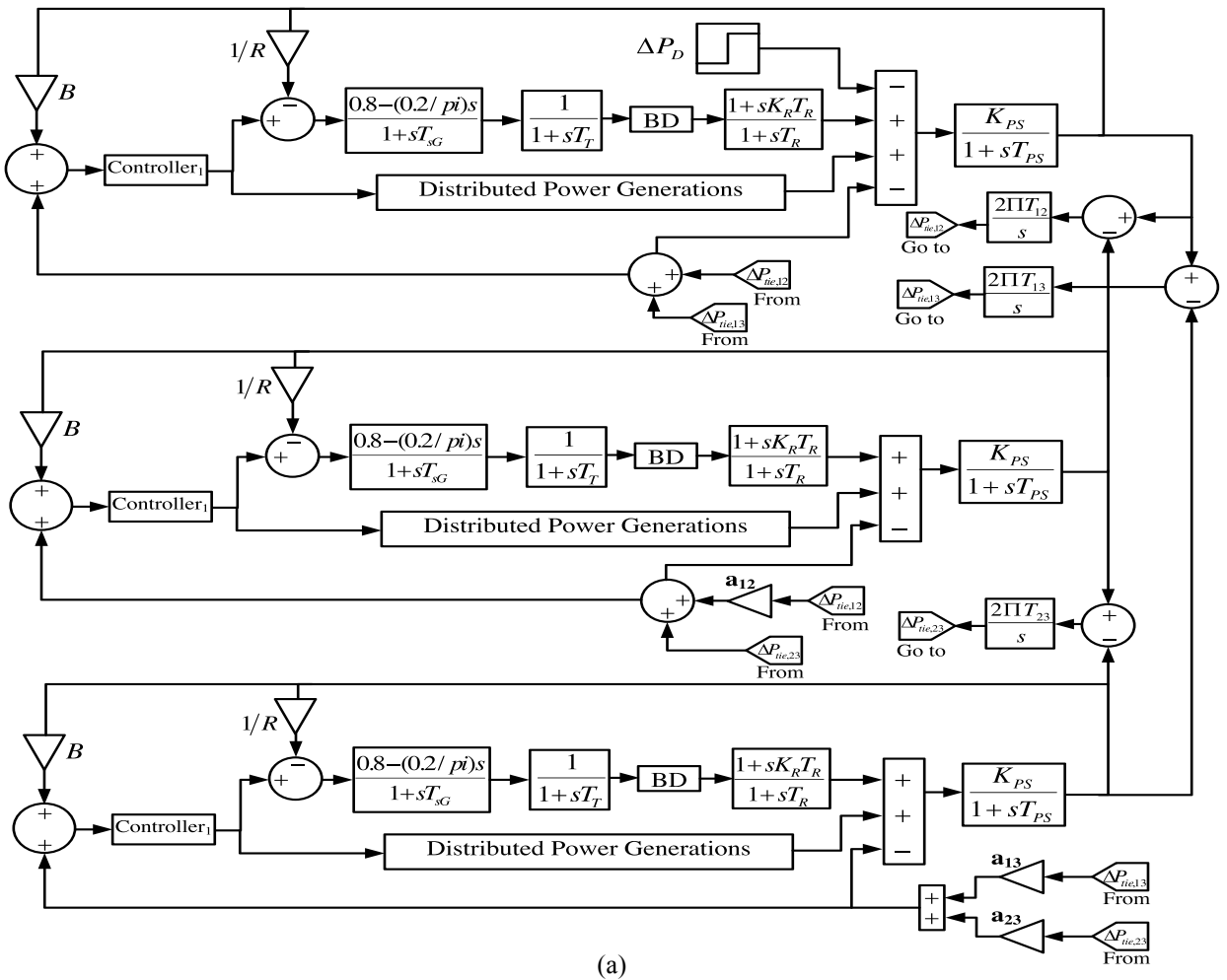


Figure 23. (a) Three-area thermal-hybrid power system, (b) transfer function model of boiler dynamics, and (c) transfer function modeling of distributed generation unit.

Table 7. Optimal parameters of PID and FPID controller tuned by different Optimization techniques.

Optimization Techniques	Gain parameters of FPID and PID controllers											
	Area-1				Area-2				Area-3			
	K ₁	K ₂	K ₃	K ₄	K ₁	K ₂	K ₃	K ₄	K ₁	K ₂	K ₃	K ₄
ADECRPSO FPID	1.1929	1.0791	1.5196	1.7456	1.3322	1.2294	1.6431	0.9320	0.5425	0.5584	1.6156	0.1776
ADECRPSO PID	0.2035	0.7463	0.6863		0.3141	0.0118	1.8690		0.5394	0.9556	0.9725	
ADE PID	0.0010	0.3532	0.8184		0.0690	0.4726	0.0010		0.8239	0.2567	1.0667	
CRPSO PID	0.0100	0.2794	0.6161		0.0918	0.0251	1.6277		0.6755	0.1132	0.1068	
DE PID	0.1727	0.1377	0.2128		0.0100	0.4156	2.0000		0.6115	0.6320	0.5945	
PSO PID	0.1201	0.0962	0.3682		0.1593	0.3654	1.8875		0.7302	0.5895	0.3274	

The performances of the system (U_{sh} , O_{sh} and T_s) are graded numerically and are tabulated in table 8. From table 8 and figures 24-26, ADECRPSO optimized FPID is superior to handle nonlinear power system model. The overall performance of proposed ADECRPSO FPID controller is better over PID controller optimized by different optimization techniques. The objective function (ITAE) is tabulated in table 9.

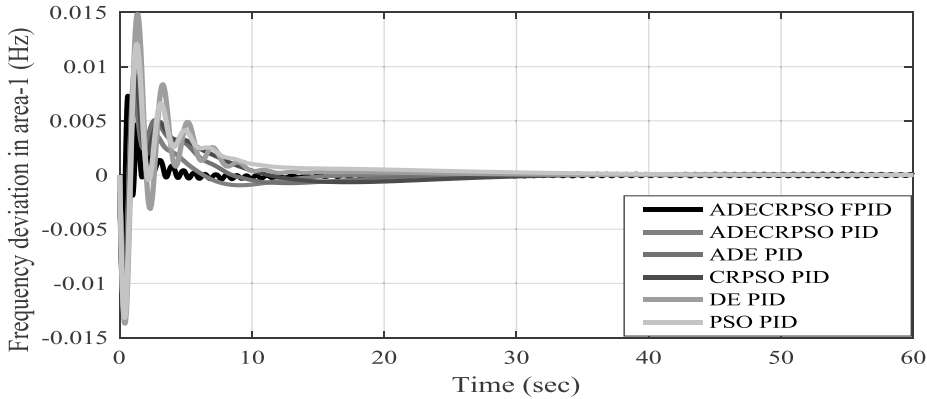


Figure 24. Frequency deviation of area1 of three-area thermal-hybrid system.

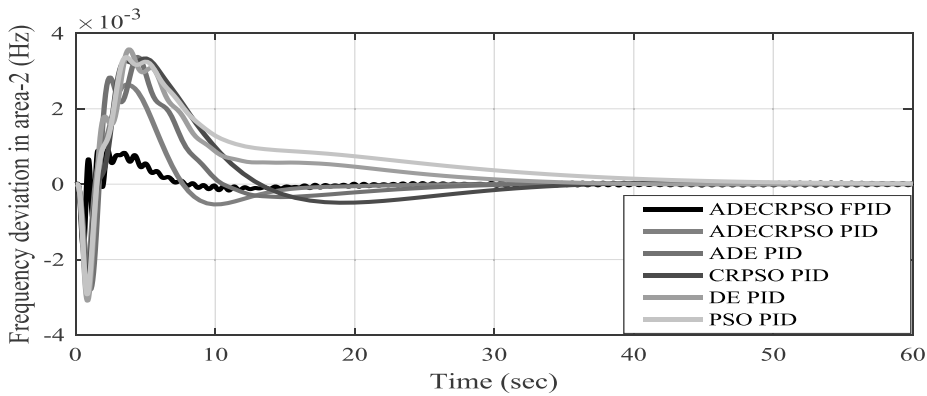


Figure 25. Frequency deviation of area 2 of three-area thermal-hybrid system.

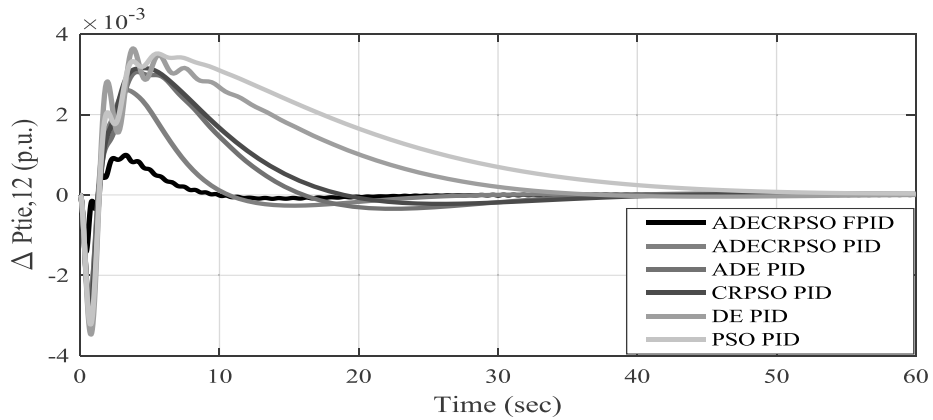


Figure 26. Tie-line power deviation between area 1 and 2 of three-area thermal-hybrid system.

Table 8. Response of the power system controlled by PID and FPID controller optimized by various algorithms.

controllers	Performance Parameters	Δf_1	Δf_2	Δf_3	$\Delta P_{tie,12}$	$\Delta P_{tie,13}$	$\Delta P_{tie,23}$	ITAE
ADECRPSO FPID	Undershoot ($U_{sh} \times 10^{-3}$)	-9.9661	-1.6242	-0.8531	-1.4175	-1.4556	-0.0090	0.01
	Overshoot ($O_{sh} \times 10^{-3}$)	7.2991	0.8964	0.8067	0.9951	1.0532	0.1457	
	Settling time (T_s)	5.79	7.69	13.55	8.71	7.77	7.55	
ADECRPSO PID	Undershoot ($U_{sh} \times 10^{-3}$)	-12.3124	-2.5946	-2.0346	-2.7381	-2.8956	-0.2697	0.9
	Overshoot ($O_{sh} \times 10^{-3}$)	9.5963	2.6419	2.5043	2.6090	2.7795	0.3457	
	Settling time (T_s)	16.91	16.91	19.39	24.95	24.95	28.55	
ADE PID	Undershoot ($U_{sh} \times 10^{-3}$)	-12.0612	-2.8012	-1.7826	-2.7062	-2.7751	-0.4104	2.2
	Overshoot ($O_{sh} \times 10^{-3}$)	7.3370	3.3552	3.0513	3.0573	3.4062	0.5868	
	Settling time (T_s)	24.22	27.72	26.55	34.71	35.87	30.05	
CRPSO PID	Undershoot ($U_{sh} \times 10^{-3}$)	-12.5129	-2.6741	-2.4176	-2.8943	-3.0785	-0.3158	2.99
	Overshoot ($O_{sh} \times 10^{-3}$)	9.1423	3.3356	3.3016	3.1541	3.4743	0.4021	
	Settling time (T_s)	30.52	33.69	33.69	37.91	38.97	38.97	
DE PID	Undershoot ($U_{sh} \times 10^{-3}$)	-13.7142	-3.0849	-2.7856	-3.4752	-3.7222	-0.3431	5.6
	Overshoot ($O_{sh} \times 10^{-3}$)	14.8325	3.5752	3.4672	3.6478	3.9736	0.4796	
	Settling time (T_s)	31.85	35.62	34.59	41.77	39.73	40.74	
PSO PID	Undershoot ($U_{sh} \times 10^{-3}$)	-13.1923	-2.9162	-2.6763	-3.2241	-3.4589	-0.3342	9.36
	Overshoot ($O_{sh} \times 10^{-3}$)	12.0856	3.3721	3.2759	3.5216	3.9896	0.4856	
	Settling time (T_s)	37.04	46.54	45.48	51.82	49.71	49.71	

CONCLUSION

In this work, a maiden endeavor is made to recommend a comparative analysis between PID and FPID controller for power/frequency stabilization of single and multi-area thermal power systems. A hybrid ADECRPSO algorithm is proposed by blending the benefits of alopex based DE and craziness based PSO algorithms. The acceptability of proposed algorithm is demonstrated over DE, PSO, CRPSO, and ADE algorithms. The basic purpose of implementation of the controller and optimization technique is to enhance the quality, reliability, and stability of the supply power to the consumers. To improve the performance of the system with same controller, the improvement of optimization technique is an indispensable factor.

A step load variation of 10% is implemented to observe the improvement of the deviation of frequency and power of the thermal-hydro-diesel power system. A comparative analysis of system performance with DE, PSO, CRPSO, ADE, and ADECRPSO algorithms optimized FPID controller is portrayed to substantiate the capability of ADECRPSO based FPID controller to yield better performance. The supremacy of FPID controller over ADECRPSO based PID controller is interpreted and it is observed that PSO based FPID is also better than ADECRPSO based PID controller. The proposed approach is substantiated in real time system (OPAL RT OP5600) and the robustness of the system is observed by implementing load variation in area-1.

Further, the analysis is extended to a two-area thermal-hydro power system with load disturbance of 1% in area-1. Hybrid ADECRPSO algorithm is ratified as an admirable technique to pursuit the PID controller gains in thermal-hydro system in comparison with hGSA-PS and hFA-PS algorithms. The proposed hybrid ADECRPSO optimized FPID controller is validated adorably with ASOS and BFOA optimized FPID controller. To substantiate the supremacy to handle non-linearity, the proposed approach is implemented in a complex thermal-hybrid power system with physical constraints. Finally, the proposed ADECRPSO algorithm and FPID controller are observed as admirable approaches to yield better performance.

APPENDIX-1 (Power system Parameters)

$T_g = 0.08$; $T_t = 0.3$; $T_r = 10$; $K_{p1} = K_{p2} = 120$; $T_{p1} = T_{p2} = 20$; $R_1 = R_2 = R_3 = 2.4$; $B_1 = B_2 = 0.425$; $T_w = 1$; $T_1 = 41.6$;
 $T_R = 5$; $T_2 = 0.513$; $K_{Diesel} = 16.5$; $a_{12} = -1$;

APPENDIX-2 (Assumptions for optimization technique)

$F = 0.65$; $CR = 0.35$; $V_{Craziness} = 0.0001$; $P_{cr} = 0.3$; $C_1 = 2.05$; $C_2 = 2.05$;

APPENDIX-3 (Hydro-thermal power system parameters)

$B_1 = 0.425$; $B_2 = 0.425$; $R_1 = 2$; $R_2 = 2.4$; $T_{h1} = 0.08$; $T_{t1} = 0.3$; $K_{p1} = K_{p2} = 100$; $T_{p1} = T_{p2} = 20$; $k_1 = 1$; $T_1 = 48.7$; $T_w = 1$; $T_2 = 0.513$; $T_r = 5$; $T_{12} = 0.0707$; $a_{12} = -1$; $\Delta P_{D1} = 0.01$; $\Delta P_{D2} = 0$;

APPENDIX-4 (Thermal-hybrid power system)

$B=0.425$; $R=2.4$; $T_{SG} = 0.08$; $T_T = 0.3$; $K_R = 0.5$; $T_R = 10$; $T_{12} = T_{23} = T_{13} = 0.0867$; $K_{PS} = 120$; $T_{PS} = 20$; $K_i=0.85$;
 $K_2=0.095$; $K_3=0.92$; $K_{IB}=0.03$; $T_{IB}=26$; $T_{RB}=6.9$; $T_F=10$; $T_D=0$; $C_B=200$; $K_{SPG} = 1$; $T_{SPG} = 1.8$; $K_{WPG} = 1$; $T_{WPG} = 1.5$; $K_{FC} = 0.01$; $T_{FC} = 4$; $K_{AE} = 0.002$; $T_{AE} = 0.5$; $K_{BESS} = -0.0033$; $T_{BESS} = 0.01$; $K_{DE} = 0.0033$; $T_{DE} = 2$; $a_{12} = -1/3$; $a_{13} = -1/5$; $a_{23} = -3/5$;

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هجين ال Alopex المبني على خوارزمية ال DECRPSO المحسن لتحكم PID الغامض لل AGC

*جيو تي رانجان نياك، *بينود شو و**بينود كومار ساهو

*قسم الهندسة الكهربائية، المعهد الوطني للتكنولوجيا، رايبور، تشهاتيسجاره، 492010، الهند.

**قسم الهندسة الكهربائية، ITER، جامعة سيكشا أنوشاندهان، بوانسوار، 751030، الهند

الخلاصة

يفضل هذا البحث ألوبيكس المستندة إلى خوارزمية تحسين الجسيمات المستندة إلى التطور التفاضلي التجزعي المستندة على خوارزميات تطور التفاضلية و معادلة تفاضلية مساعدة و تحسين سرب الجسيمات و تحسين سرب الجسيمات المستند إلى التجزع لمتابعة معلمات الكسب بوحدة التحكم التناسبي الذي لا يتجزأ و تحسين سرب الجسيمات الغامضة. في نظام طاقة حراري يعمل بالديزل في منطقتين ، يتم اعتماد أولوية وحدة التحكم تحسين سرب الجسيمات المستند إلى التجزع مع وحدة تحكم تناسبي لا يتجزأ تم ضبطها بتقنيات تحسين متنوعة. تم تأكيد خوارزمية تحسين الجسيمات المستندة إلى التطور التفاضلي التجزعي الهجينة على الخوارزميات المذكورة أعلاه لضبط وحدة تحكم و وحدة تحكم تناسبي لا يتجزأ في نظامين مائي حراري. يتم تنفيذ كل من تحسين سرب الجسيمات و تطور التفاضلية و تحسين سرب الجسيمات المستند إلى التجزع و معادلة تفاضلية مساعدة و خوارزمية تحسين الجسيمات المستندة إلى التطور التفاضلي التجزعي بشكل فردي لتحسين وحدة التحكم لتعزيز التحليل العابر عن طريق التنازل عن القاع ، والخطأ الزائد ، واستقرار وقت النظام. يؤدي تجميع مزايا تطور التفاضلية المستندة إلى ألوبيكس و تحسين سرب الجسيمات المستندة إلى التجزع إلى خوارزمية هجينة كافية تعزز أداء التحكم التلقائي في التوليد. يتم فرض زيادة حمل الخطوة في المنطقة 1 لمراقبة أنشطة التحكم التلقائي في التوليد. لا يمكن إنكاره أن وحدة تحكم و وحدة تحكم التناسبي الذي لا يتجزأ المحسنة من قبل خوارزمية تحسين الجسيمات المستندة إلى التطور التفاضلي التجزعي تلتزم بأداء فائق على وحدة تحكم تحسين سرب الجسيمات و تطور التفاضلية و تحسين سرب الجسيمات المستند إلى التجزع و معادلة تفاضلية مساعدة المحسنة كنظام التحكم التلقائي في التوليد المقترح. تتحقق وحدة التحكم التناسبي الذي لا يتجزأ المحسنة بواسطة خوارزمية تحسين الجسيمات المستندة إلى التطور التفاضلي التجزعي و معادلة تفاضلية مساعدة و خوارزمية تحسين الجسيمات التجزعية في بيئة الوقت الفعلي (OPAL RT OP5600). لذلك ، فإن طفرة معدلة من تطور التفاضلية بواسطة ألوبيكس مخطط يعزز القدرة على ضبط متغيرات النظام.